

Name:	 <b>UPES</b> UNIVERSITY WITH A PURPOSE
Enrolment No:	

**UNIVERSITY OF PETROLEUM AND ENERGY STUDIES**

End Semester Examination, May 2019

Course: Chemical Engineering Thermodynamics-II

Semester: IV

Program: B.Tech CERP & APE-Gas

Time 03 hrs.

Course Code: CHCE-2008

Max. Marks: 100

**Instructions:**

**SECTION A**  
(30 marks)

S. No.	Question	Marks	CO
Q 1	<p>(a) Explain the significance of <b>Virial coefficients</b></p> <p>(b) Differentiate between <b>Two-parameter</b> and <b>Three-parameter</b> correspondence state theorems</p>	4  4	CO1
Q 2	<p><b>Water (1) – hydrazine (2)</b> system forms an azeotrope containing <b>58.5 % (mol)</b> hydrazine at <b>393 K</b> and <b>101.3 kPa</b>. Calculate the equilibrium vapor composition for a solution containing <b>20 % (mol)</b> hydrazine. The relative volatility of water with reference to hydrazine is <b>1.6</b>, is assumed to remain constant in the temperature range involved. The vapor pressure of Hydrazine at <b>393 K</b> is <b>124.76 kPa</b>. Use <b>Van laar model</b>.</p> <p><math>A = \ln \gamma_1 (1 + x_2 \ln \gamma_2 / x_1 \ln \gamma_1)^2</math>      <math>B = \ln \gamma_2 (1 + x_1 \ln \gamma_1 / x_2 \ln \gamma_2)^2</math></p>	8	CO4
Q 3	<p><b>Deduce Gibbs – Duhem</b> equation for a binary system <b>Chemical Potential</b> and also in terms of <b>activity &amp; activity coefficient</b></p>	7	CO3
Q 4	<p><b>Classify</b> types of common adsorbents and <b>discuss</b> their characteristics</p>	7	CO5

**SECTION B**  
45 marks

Q 7	<p>(a) <b>Interpret</b> the following semi-empirical models in thermodynamics</p> <p>(i) <b>Margules 3-suffix</b> model</p> <p>(ii) <b>Van laar</b> model</p> <p>(b) <b>Perform VLE</b> calculations for the <b>Methane (1)/ Ethylene (2) / Ethane (3)</b> system using <b>K-values</b></p> <p>(i) <b>BUBL P</b>, given <math>x_1 = 0.1</math>, <math>x_2 = 0.5</math> and <math>T = 222.15</math> K</p> <p>(ii) <b>BUBL T</b>, given <math>x_1 = 0.12</math> and <math>x_2 = 0.4</math> and <math>P = 17.24</math> bar</p>	8      7	CO4
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Q 8	<p>The excess Gibbs energy of a binary liquid mixture at T &amp; P is given by,</p> $G^E / RT = (-2.6x_1 - 1.8x_2) x_1 x_2$ <p>(i) Find expression for <math>\ln \gamma_1</math> &amp; <math>\ln \gamma_2</math> at T &amp; P</p> <p>(ii) Show that these expressions satisfy <b>Gibbs-Duhem</b> equation in terms of activity coefficients.</p> <p>(iii) Show that <math>(d \ln \gamma_1 / dx_1)_{x_1=1} = (d \ln \gamma_2 / dx_1)_{x_1=0} = 0</math></p> <p>(iv) Plot <math>G^E/RT</math>, <math>\ln \gamma_1</math> and <math>\ln \gamma_2</math> as calculate by the given equation for <math>G^E/RT</math> and by the equation developed in (i) vs <math>x_1</math>.</p>	15	CO3
Q 9	<p>The molar volume <math>\text{cm}^3 \text{mol}^{-1}</math> of a binary liquid mixture at T and P is given by,</p> $V = 120x_1 + 70 x_2 + (15 x_1 + 8 x_2) x_1 x_2$ <p>(i) Find the expression for the partial molar volume of species 1 &amp; 2 at T and P.</p> <p>(ii) Show this equation satisfy the <b>Gibbs-Duhem</b> equation in terms of partial molar volumes.</p> <p>(iii) Find the values of V, partial molar volume of species 1 &amp; 2</p> <p>(iv) Show that <math>(dV_1/dx_1)_{x_1=1} = (dV_2/dx_1)_{x_1=0} = 0</math></p>	15	CO3
<b>SECTION-C</b> <b>1 x 25 = 25 marks</b>			
Q 10	<p>For the <b>Acetone (1) / Methanol (2)</b> system a vapor mixture for which, <math>z_1 = 0.25</math> and <math>z_2 = 0.75</math> is cooled to temperature T in the two-phase region and flow into a separation chamber at a pressure of <b>1 bar</b>. If the composition of liquid product is to be <math>x_1 = 0.175</math>, what is the required value of T and what is the value of <math>y_1</math>? For liquid mixtures of the system to a good approximation</p> $\ln \gamma_1 = 0.64 x_2^2 \qquad \ln \gamma_2 = 0.64 x_1^2$ <p><b>Acetone (1) : A = 14.3916, B = 2795.82 and C = 230</b>  <b>Methanol (2) : A = 16.5938, B = 3644.3 and C = 239.76</b></p> <p style="text-align: center;"><b>OR</b></p> <p>A process stream contains light species “1” and heavy species “2”. A relative pure</p>	25	CO4

liquid stream containing mostly **2** is desired obtained by a single-stage liquid and vapor separation. Specifications on the equilibrium composition are  $x_1 = 0.002$  and  $y_1 = 0.950$ . Use data given below to determine **T (K)** and **P (bar)** for the separator. Assume modified **Raoult's** law is applies, the calculated **P** should validate this assumption.

For liquid phase,  $\ln\gamma_1 = 0.93 x_2^2$                        $\ln\gamma_2 = 0.93 x_1^2$

$$\ln P_i^{sat} / \text{bar} = A_i - B_i/T(\text{K})$$

**$A_1 = 10.08$ ,  $B_1 = 2572.0$ ,  $A_2 = 11.63$  and  $B_2 = 6250$**

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**Instructions:**

**SECTION A  
(30 marks)**

S. No.		Marks	CO
Q 1	<b>Deduce</b> an expression for <b>Pitzer</b> correlation for Second Virial Coefficient	8	CO1
Q 2	Under atmospheric conditions, the <b>Acetone (1)-Chloroform (2)</b> azeotrope boils at <b>64.6°C</b> and contains <b>33.5 mol. %</b> Acetone. The vapor pressure of Acetone and Chloroform at this temperature are <b>995 mmHg</b> and <b>885 mmHg</b> respectively. Calculate the composition of the vapor at this temperature in equilibrium with a liquid analyzing <b>11.1 mol. %</b> Acetone. Apply <b>Van laar</b> equations of the following form:  $A = \ln\gamma_1 ( 1 + x_2 \ln\gamma_2/x_1 \ln\gamma_1 )^2 \quad B = \ln\gamma_2 ( 1 + x_1 \ln\gamma_1/x_2 \ln\gamma_2 )^2$	8	CO4
Q 3	<b>Deduce Gibbs – Duhem</b> equation for a binary system <b>Chemical Potential</b> and also in terms of <b>activity &amp; activity coefficient</b>	7	CO3
Q 4	<b>Classify</b> types of common adsorbents and <b>discuss</b> their characteristics	7	CO5

**SECTION B  
45 marks**

Q 7	(a) <b>Interpret</b> the following semi-empirical models in thermodynamics  (iii) <b>Margules 3-suffix</b> model (iv) <b>Van laar</b> model  (c) <b>Perform VLE</b> calculations for the <b>Methane (1)/ Ethylene (2) / Ethane (3)</b> system using <b>K-values</b> (iii) <b>DEW P</b> , given $y_1 = 0.5$ , $y_2 = 0.25$ and $T = 222.15$ K (iv) <b>DEW T</b> , given $y_1 = 0.43$ and $y_2 = 0.36$ and $P = 17.24$ bar	8       7	CO4
Q 8	<b>Derive</b> the expressions for $G^{id}$ , $S^{id}$ , $V^{id}$ and $H^{id}$ for Ideal solutions mixtures with proper assumptions	15	CO3
Q 9	For a binary liquid mixture at $T$ and $P$ , the molar volume is given by,  $V = 120x_1 + 70 x_2 + (15 x_1 + 8 x_2) x_1 x_2$  (v) <b>Deduce</b> the expression for the partial molar volume of species <b>1 &amp; 2</b> at $T$	15	CO3

	<p>and P.</p> <p>(vi) <b>Prove</b> the equation satisfy the <b>Gibbs-Duhem</b> equation in terms of partial molar volumes.</p> <p>(vii) Show the values of V, partial molar volume of species <b>1 &amp; 2</b></p> <p>(viii) Show that <math>(d\hat{V}_1/dx_1)_{x_1=1} = (d\hat{V}_2/dx_1)_{x_1=0} = 0</math></p>		
<b>SECTION-C</b> <b>1 x 25 = 25 marks</b>			
<b>Q 10</b>	<p>A system consists of a vapor mixture of <b>Acetone (1) / Methanol (2)</b> in which, <math>z_1 = 0.35</math> and <math>z_2 = 0.65</math> is cooled to temperature <b>T</b> in the two-phase region and flow into a separation chamber at a pressure of <b>1 bar</b>. If the composition of liquid product is to be <math>x_1 = 0.275</math>, what is the required value of <b>T</b> and what is the value of <math>y_1</math>? For liquid mixtures of the system to a good approximation</p> $\ln \gamma_1 = 0.63 x_2^2 \qquad \qquad \qquad \ln \gamma_2 = 0.63 x_1^2$ <p><b>Acetone (1) : A = 14.3916, B = 2795.82 and C = 230</b>  <b>Methanol (2) : A = 16.5938, B = 3644.3 and C = 239.76</b></p> <p style="text-align: center;"><b>OR</b></p> <p>A process stream contains light species “1” and heavy species “2”. A relative pure liquid stream containing mostly <b>2</b> is desired obtained by a single-stage liquid and vapor separation. Specifications on the equilibrium composition are <math>x_1 = 0.002</math> and <math>y_1 = 0.950</math>. Use data given below to determine <b>T (K)</b> and <b>P (bar)</b> for the separator. Assume modified <b>Raoult’s</b> law is applies, the calculated <b>P</b> should validate this assumption.</p> <p>For liquid phase, <math>\ln \gamma_1 = 0.64 x_2^2 \qquad \qquad \qquad \ln \gamma_2 = 0.64 x_1^2</math></p> $\ln P_1^{sat} / \text{bar} = A_i - B_i/T(\text{K})$ <p><b>A<sub>1</sub> = 10.08, B<sub>1</sub> = 2572.0, A<sub>2</sub> = 11.63 and B<sub>2</sub> = 6250</b></p>	<b>25</b>	<b>CO4</b>