Name:

Enrolment No:



UNIVERSITY WITH A PURPOSE

UNIVERSITY OF PETROLEUM AND ENERGY STUDIES End Semester Examination, December 2021

Course: Gas Dynamics and Jet Propulsion Program: B.Tech ASE, ASE+AVE Course Code: ASEG 4014

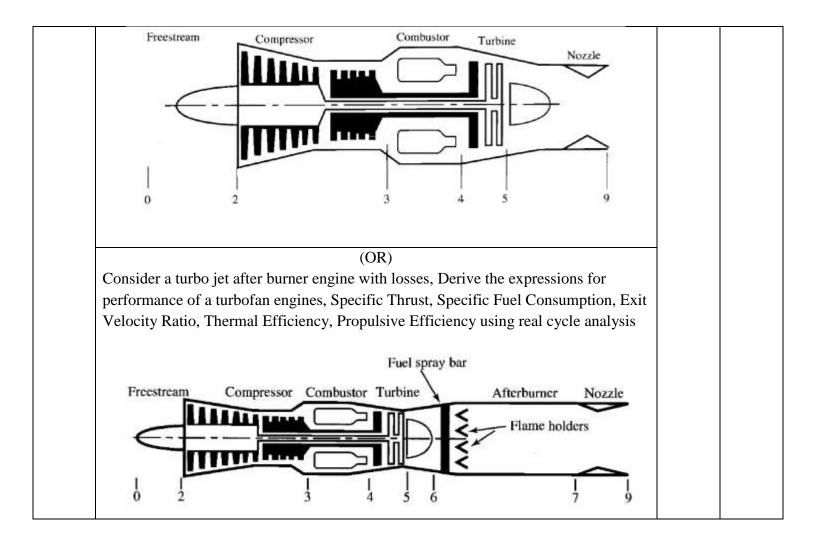
Semester: VII Time 03 hrs. Max. Marks: 100

Number of pages: 11

Instructions: Isentropic, Shock tables, Fanno tables, Ryleigh tables are included SECTION A

S. No.		Marks	CO
Q 1	What are oblique shock intakes? Does the stagnation pressure loss for such inlet greater than an inlet with a single normal shock.	4	CO2
Q 2	Explain about subsonic inlets, Inlet drag and inlet distortion and explain about its effect on inlet design and performance in aircraft engines?	4	CO1
Q 3	Demonstrate the assumptions of ideal Cycle Parametric Cycle Analysis for various Engines, also comment on the Real cycle Analysis consideration on component efficiencies.	4	CO2
Q 4	Explain the process of combustion in gas turbine combustion chamber, Illiterate using a Jet engine Burner and bring out the various zones that play major role in the process of combustion?	4	CO1
Q 5	Explain the performance improvements of adding afterburner in turbojet when compared with ideal turbojet without afterburner.	4	CO1
	SECTION B		
Q 6	Air at inlet to an insulated constant area duct of diameter 160 mm has a Mach number of 0.36. The mean friction factor of the duct for the flow conditions is 0.0025. What length of the pipe would give a 10% loss in stagnation pressure? What is the Mach number at the corresponding exit section? What is percentage loss in stagnation pressure, if the flow extends to sonic condition?	10	CO3
Q 7	A gaseous Mixture of air and fuel enters a ramjet combustion chamber with velocity 60 m/s, temperature 50 °C and pressure 35 kPa. The heat of reaction of the mixture for the particular fuel air ration employed is 1160 kJ/kg. Find the condition of stream at the exit of combustion chamber, if friction is neglected and the cross sectional area is assumed constant. Assume the properties of both reactants and products of combustion are the same as air.	10	CO2

Q 8	Explain about Nacelle and Interference Drag and types of flow configurations in the		
	diffusers. Explain about the challenges in Supersonic intakes design for fighter		
	aircrafts.	10	CO4
Q 9	Consider the combustion chamber in a jet engine at cruising altitude. For simplicity,		
	the combustor is operated at 1 atm of pressure and burns a stoichiometric (ϕ =0.92)		
	mixture of n-heptane (C7H16) and air. The intake conditions are as indicated below		
	Fuel: $T_{fuel} = 25^{\circ}C$ $P_{fuel} = 1 atm$ Air: $T_{air} = 427^{\circ}C$ $P_{air} = 1 atm$ \dot{Q}_{loss} \dot{Q}_{loss}		
	(a). Write the stoichiometric chemical reaction for the fuel with air.	10	CO2
	(b) If the mass flow rate of fuel is 1 kg/s, what is the mass flow rate of air?		
	(OR)		
	A convergent- divergent nozzle operating with inlet conditions of 4 bar and 450° C		
	with negligible inlet velocity, is expected to give an exit static pressure of 1 bar		
	under ideal conditions. Estimate the exit temperature and Mach number assuming		
	nozzle efficiency of 0.92. The expansion takes place to the same exit pressure as in		
	the ideal case. Take air as the working fluid?		
	SECTION-C		
Q 10	(a). An aircraft engine employs a subsonic inlet diffuser of area ratio 4. Free stream		
QIU	(a). An alrefait engine employs a subsolic linet diffuser of area ratio 4. Free stream air at a total pressure and temperature of 1×10^5 N/m ² and 570 K approaches the diffuser with a Mach number 2.2. A shock wave stands just outside the diffuser inlet. Determine the Mach number, pressure and temperature of the air at the exit of the diffuser. Also fine the loss in stagnation pressure of air. (b)Explain how does a shock wave develop in the diverging section of a supersonic nozzle. When does this wave move towards the exit?	15+5	CO4
Q 11	Derive the expressions for performance in Turbojet using parametric cycle analysis by considering ideal process.	20	CO5



0.80	0.78	0.76	0.74	0.72	e.	0.70	0.68	0.66	0.64	0.62		0.60	0.58	0.56	0.54	0.52	5	0.50	0.48	0.46	0.44	0.42	a,	0.40	0.38	0.36	0.34	0.32	1	0.30	0.28	0.26	0.24	0.22	0.20	0.00	0.10	0.14	0.12		0.10	0.08	0.06	0.04	0.02	ME
0.8865	0.8915	0.8964	0.9013	0.9061		0.9107	0.9153	0.9199	0.9243	0.9286		0.9328	0.9370	0.9410	0.9449	0.9487		0.9524	0.9559	0.9594	0.9627	0.9659	1	0.9690	0.9719	0.9747	0.9774	0.9799	1	0.9823	0.9846	0.9867	0.9886	0.9904	0.7744	0.0001	0.9949	1066.0	1/66/0	1007	0.9980	0.9987	0.9993	0.9997	6666'0	T/T_0
0.6560	0.6691	0.6821	0.6951	0.7080		0.7209	0.7338	0.7465	0.7591	0.7716		0.7840	0.7962	0.8082	0.8201	0.8317	1996-900 200	0.8430	0.8541	0.8650	0.8755	0.8857		0.8956	0.9052	0.9143	0.9231	0.9315	19	0.9395	0.9470	0.9541	0.9607	0.9668		0.0700	0.9020	0.0000	UN6671	-	0.9930	0.9955	0.9975	0.9989	0.9997	Pala
1.0382	1.0471	1.0570	1.0681	1.0806		1.0944	1.1097	1.1265	1.1451	1.1656		1.1882	1.2130	1.2403	1.2703	1.3034	•	1.3398	1.3801	1.4246	1.4740	1.5289	3	1.5901	1.6587	1.7358	1.8229	1.9219	1	2.0351	2.1656	2 3173	2.4956	2.7076		3020 0	3.0720	4.1024	Choort-	10/10	5.8218	7.2616	9.6659	14.4815	28.9421	A/A-
0.6811	0.7005	0.7209	0.7424	0.7651	1	0.7890	0.8142	0.8410	0.8693	566870	-	0.9316	0.9658	1.0024	1.0417	1.0840		1.1295	1.1788	1.2322	1.2905	1.3542	ï	1.4242	1.5014	15871	1.6827	1.7902	1	1.9119	2.0508	2 2109	2 3975	2.6178		0000 0	2 20017	00110	OCTOR	- 0182	5.7813	7.2292	9.6416	14.4653	28.9340	100 lun
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160	158	1.56	154	1.52	1	1.50	1.48	1.46	1.44	1.42		1.40	1.38	1.36	1.34	1.32		1.30	1.28	1.26	1.24	1.22	1	1.20	1.18	1.16	1.14	1.12	1	1.10	1.08	106	104	1.02	1.00	100	0.08	0.94	26.0	» ,	0.90	88.0	0.86	0.84	0.82	IM
0.6614	0.6670	0.6726	0.6783	0.6840	-	0.6897	0.6954	0.7011	0.7069	0.7126		0.7184	0.7242	0.7300	0.7358	0.7416		0.7474	0.7532	0.7590	0.7648	0.7706	x	0.7764	0.7822	0.7879	0.7937	0.7994	1	0.8052	0.8108	0.8165	0.8222	0.8278	Property in	00000	0.8380	0.0490	700010	1 0000	0.8606	0.8659	0.8711	0.8763	0.8815	0112
0.2353	0.2423	0.2496	0.2570	0.2646		0.2724	0.2804	0.2886	0.2969	650E.0		0.3142	0.3232	0.3323	0.3417	0.3512		0.3609	0.3708	0.3809	0.3912	0.4017	1	0.4124	0.4232	0.4343	0.4455	0.4568		0.4684	0.4800	0.4919	0.5039	0.5160	0.0000	0 2000	0 5407	ococ.u	02/20	-	0.5913	0.6041	0.6170	0.6300	0.6430	0.112
1.2502	1.2344	1.2190	1.2042	1.1899	1	1.1762	1.1629	1.1501	1.1379	1.1262		1.1149	1.1042	1.0940	1.0842	1.0750		1.0663	1.0581	1.0504	1.0432	1.0366	4	1.0304	1.0248	1.0198	1.0153	1.0113	-	1.0079	1.0051	1.0029	1.0013	1.0003		1 0000	1,0001	TCOOL	OCULL	1 0022	1.0089	1.0129	1.0179	1.0237	1.0305	when
0.2941	0.2991	0.3042	0.3095	0.3149	and a state of the	0.3204	0.3261	0.3319	0.3379	0.3440		0.3504	0.3569	0.3636	0.3704	0.3775	•	0.3848	0.3924	0.4001	0.4081	0.4164	1	0.4249	0.4337	0.4428	0.4523	0.4620		0.4721	0.4825	0.4933	0.5045	0.5162	0	00000	0.5200	0,000	1100.0		0.5965	0.6119	0.6281	0.6449	0.6626	would a
38 682	39.265	39.868	40.493	41.140		41.810	42.507	43.230	43.983	44.767		45.585	46.439	47.332	48.268	49.251		50.285	51.375	52.528	53,751	55.052	1	56.443	57.936	59.550	61.306	63.234	i	65.380	67.808	70.630	74.058	78.635		00.000		3	110	ŝ	ΞX	63	7	5	x:	1
14.860	14.269	13.677	13.086	12.495	100	11.905	11.317	10.731	10.146	695.6		8.987	8.413	7.844	7.279	6.721	ł	6,170	5.627	5.093	4.569	4.057	1	3.558	3.074	2.607	2.160	1.735		1.336	0.968	0.637	0.351	0.126	0000	0,000	23	3	823	ĩ	97	P	a.	2	75	4
240	2 38	2.36	234	2.32	,	2.30	2.28	2.26	2.24	2.72		2.20	218	2.16	2.14	212	,	210	2.08	2.06	2.04	2.02	4	2.00	1.98	1.96	1.94	1.92	÷	1.90	1.88	18	184	1.82		100	178		177	; ·	1.70	1.68	1.66	1.64	1.62	INT
0.4647	0.4688	0.4731	0.4773	0.4816	1	0.4859	0.4903	0.4947	0.4991	0.5036	-	0.5081	0.5127	0.5173	0.5219	0.5266		0.5313	0.5361	0.5409	0.5458	0.5506	•	0.5556	0.5605	0.5655	0.5705	0.5756	13	0.5807	0.5859	0.5910	0.5963	0.6015		0.00121	C/10/0	677010	0.0200	-	0.6337	0.6392	0.6447	0.6502	0.6558	0111
0.0684	0.0706	0.0728	0.0751	0.0775		0.0800	0.0825	0.0851	0.0878	0.0906	-	0.0935	0.0965	0.0996	0.1027	0.1060		0.1094	0.1128	0.1164	0.1201	0.1239	x	0.1278	0.1318	0.1360	0.1403	0.1447		0.1492	0.1539	0.1587	0.1637	0.1688	0.11 M	0.1710	0.1000	0.1907	0.1900	-	0.2026	0.2088	0.2151	0.2217	0.2284	0.1/4
2 4031	2 3593	2.3164	2.2744	2.2333		2.1931	2.1538	2.1153	2.0777	2.0409	-	2.0050	1.9698	1.9354	1.9018	1.8690		1.8369	1.8056	1.7750	1.7451	1.7160		1.6875	1.6597	1.6326	1.6062	1.5804		1.5553	1.5308	1 5069	1.4836	1.4610	ALCON.	1 4000	1.0907	10/01	1.0004	+ 382.7	1.3376	1.3190	1.3010	1.2836	1.2666	when
0.1644	0.1665	0.1687	0.1709	0.1731		0.1754	0.1777	0.1801	0.1825	0.1850		0.1875	0.1901	0.1927	0.1954	0.1981	,	0.2009	0.2037	0.2066	0.2096	0.2126	5	0.2157	0.2188	0.2220	0.2253	0.2287		0.2321	0.2356	0.2392	0.2429	0.2466		0.000	0.2204	0.2020	0.2007	-	0.2710	0.2754	0.2799	0.2845	0.2893	walnu
24.624	24.845	25.070	25.300	25.533	(25.771	26.014	26.262	26.515	26.773		27.036	27.304	27.578	27.859	28.145		28.437	28.736	29.041	29.353	29.673	1	30.000	30.335	30.677	31.028	31.388	1	31.757	32.135	32 523	32.921	33.329		22 740	120.00	30,000	600.30		36.032	36.530	37.043	37.572	38.118	, pr
36.747	36.261	35.771	35.279	34.782		34.283	33.780	33.273	32.763	32.249						29.631			28.560				7				24.712	24.151	F	23.586				21.302			201146			+0.900	17.810				15.452	v

Table A.1: Isentropic flow properties for $\gamma = 1.4$

Table A.2: Isentropic flow properties for $\gamma = 1.4$

	M2	T2/T1	P2/P1	Pog/Pot	P02/P1	$\Delta V/a_1$	M ₁	M2	T2/T1	P2/P1	P02/P01	P02/P1	ΔV/a1	M ₁	M2	3 12		T_2/T_1	T2/T1 P2/P1	T2/T1 P2/P1 Pc2/P01
1.02	0.9805	1.0132	1.0471	1.0000	1.9379	0.033	1.82	0.6121	1.5466	3.6978	0.8038	4.7618		1,059	_	_	2.62	2.62 0.5022	2.62 0.5022 2.2590	2.62 0.5022 2.2590 7.8418
	0.9444	1.0393	1.1442	86660	2.0325	0.097	1.86	0.6036	1.5770	3.8695	0.7857	4.9497	1422	1,102		2.66	2.66 0.4988	2.66 0.4988 2.3006	2.66 0.4988 2.3006 8.0882	2.66 0.4988 2.3006 8.0882 0.4379
1.08	0.9277	1.0522	1.1941	0.9994	2.0819	0.128	1.88	0.5996	1.5924	3.9568	0.7765	5.0452		1.123	123 2.68	0.50	2.68	2.68 0.4972	2.68 0.4972 2.3217	2.68 0.4972 2.3217 8.2128
	0.24.00	1.000		-000		0.107		Arrest and	- 1001	action of		And a state of the					00000	Canada Canada Canada		and another and and and
1.12	0.8966	1.0776	1.2968	0.9982	2.1851	0.189	1.92	0.5918	1.6236	4.1341	0.7581	5.2394	1	.166			2.72	2.72 0.4941	2.72 0.4941 2.3642 8.4648 0.4	2.72 0.4941 2.3642 8.4648 0.4166
	0.8820	1.0903	1.3495	0.9973	2.2388	0.219	1.94	0.5880	1.6394	4.2242	0.7488	5.3381		1187	1.187 2.74	2.74	2.74	2.74 0.4926 2.3858	2.74 0.4926 2.3858 8.5922	2.74 0.4926 2.3858 8.5922
	0.8549	1.1154	1.4578	0.9946	2 3500	0.277	1.98	0.5808	1.6713	4.4071	0.7302	5.5386		1.229			2.78 0.4896	2.78 0.4896	2.78 0.4896 2.4292	2.78 0.4896 2.4292 8.8498 0.3961
1.20	0.8422	1.1280	1.5133	0.9928	2.4075	0.306	2.00	0.5774	1.6875	4.5000	0.7209	5.6404		1.250		2.80	2.80 0.4882	2.80 0.4882 2.4512	2.80 0.4882 2.4512 8.9800	2.80 0.4882 2.4512 8.9800 0.3895
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1.22	0.8300	1.1405	1.5698	206670	2.4663	0.334	2.02	0.5740	1.7038	4.5938	0.7115	5.7433		1.271	20	2.82	2.82 0.4868	2.82 0.4868 2.4733	2.82 0.4868 2.4733 9.1111	2.82 0.4868 2.4733 9.1111
	0.8183	1.1531	1.6272	0.9884	2.5263	0.361	2.04	0.5707	1.7203	4.6885	0.7022	5.8473	10		1.292	1.292 2.84	1.292 2.84 0.4854	1.292 2.84 0.4854 2.4955	1.292 2.84 0.4854 2.4955 9.2432	1.292 2.84 0.4854 2.4955 9.2432 0.3765
	0.8071	1.1657	1.6855	0.9857	2.5875	0.389	2.06	0.5675	1.7369	4.7842	0.6928	5.9523				1.312 2.86	1.312 2.86 0.4840	1.312 2.86 0.4840 2.5179	1.312 2.86 0.4840 2.5179 9.3762	1.312 2.86 0.4840 2.5179 9.3762 0.3701
	0.7860	1.1909	1.8050	0.9794	27136	0.442	210	0.5613	1.7305	4.9783	0.6742	6.1654		1.23	1353	1353	1353 2.90	1.353 2.90 0.4814	1.353 2.90 0.4814 2.5632	1.353 2.90 0.4814 2.5632 9.6450
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134	0.7664	1.2162	1.9282	0.9718	28444	0.495	2.14	0.5554	1.8046	5.1762	0.6557	6.3827		1394			2.94	2.94 0.4788	2.94 0.4788 2.6091	2.94 0.4788 2.6091 9.9175
	0.7572	1.2290	1.9912	0.9676	29115	0.521	2.16	0.5525	1.8219	5.2765	0.6464	6.4929		1.414		2.96	2.96 0.4776	2.96 0.4776 2.6322	2.96 0.4776 2.6322 10.0552	2.96 0.4776 2.6322 10.0552 0.3398
1.30	0.7307	1 2547	10001 0	0.0580	3 0400	0.540	2 20	0.5471	1 9540	5 4800	0.6281	67165		1.455			105	2.00 0.4752	3.00 0.4752 2.6700	2.90 0.4764 2000 10 2223 3.00 0.4764 2000 10 2233
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	0.7314	1.2676	2.1858	0.9531	3.1198	0.596	2.22	0.5444	1.8746	5.5831	0.6191	6.8298		1.475		3.02	3.02 0.4740	3.02 0.4740 2.7026	3.02 0.4740 2.7026 10.4738	3.02 0.4740 2.7026 10.4738 0.3227
	0.7235	1.2807	2.2525	0.9476	3.1915	0.621	2.24	0.5418	1.8924	5.6872	0.6100	6.9442		1.495	1.495 3.04	3.04	3.04 0.4729	3.04 0.4729	3.04 0.4729 2.7264	3.04 0.4729 2.7264 10.6152 0.3172
148	0.7083	1.3069	2 3888	0.9360	3,3382	0.670	2.28	0.5368	1.9285	5.8981	0.5921	7.1762		1535			3.08	3.08 0.4706 2.7744	3.08 0.4706 2.7744 10.9008	3.08 0.4706 2.7744 10.9008
	0.7011	1.3202	2,4583	0.9298	3.4133	0.694	2.30	0.5344	1.9468	6.0050	0.5833	7.2937		1.554		3.10	3.10 0.4695	3.10 0.4695 2.7986	3.10 0.4695 2.7986 11.0450	3.10 0.4695 2.7986 11.0450 0.3012
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	1969-0	1.3336	2.5288	0.9233	3.4894	0.718	2.32	0.5321	1.9652	6.1128	0.5745	7.4122		1.574	25	3.12	3.12 0.4685	3.12 0.4685 2.8230	3.12 0.4685 2.8230 11.1901	3.12 0.4685 2.8230 11.1901 0.2960
	0.6809	1.3606	2.6725	0.9097	3.6450	0.766	2.36	0.5275	2.0025	6.3312	0.5572	7.6525		1.614			3.16	3.16 0.4664	3.16 0.4664 2.8722	3.16 0.4664 2.8722 11.4832
1.58	0.6746	1.3742	2.7458	0.9026	3.7244	0.789	2.38	0.5253	2.0213	6.4418	0.5486	7.7742		1.633		3.18	3.18 0.4654	3.18 0.4654 2.8970 1	3.18 0.4654 2.8970 11.6311	3.18 0.4654 2.8970 11.6311 0.2811
	0.6684	1.3880	2.8200	0.8952	3,8050	0.813	2.40	0.5231	2.0403	6.5533	0.5401	7.8969		1.653	1.653 3.20	3.20	3.20 0.4643	3.20 0.4643 2.9220	3.20 0.4643 2.9220 11.7800	3.20 0.4643 2.9220 11.7800 0.2762
	0.6625	1.4018	2.8951	0.8877	3.8866	0.836	2.42	0.5210	2.0595	6.6658	0.5317	8.0207		1.672		3.22	3.22 0.4634	3.22 0.4634 2.9471 1	3.22 0.4634 2.9471 11.9298	3.22 0.4634 2.9471 11.9298 0.2715
	0.6568	1.4158	2.9712	0.8799	3.9693	0.859	244	0.5189	2.0788	6.7792	0.5234	8.1455		1.692		3.24	3.24 0.4624	3.24 0.4624 2.9724	3.24 0.4624 2.9724 12.0805	3.24 0.4624 2.9724 12.0805 0.2668
	0.6458	14440	3 1261	0.8639	4.1379	0.904	248	0.5149	2.1178	7.0088	05071	8 3982		1731			3.28 0.4605	3.28 0.4605	3.28 0.4605 3.0234 12.3848	3.28 0.4605 3.0234 12.3848
1.70	0.6405	1.4583	3.2050	0.8557	4.2238	0.926	2.50	0.5130	2.1375	7.1250	0.4990	8.5261		1.750		3.30	3.30	3.30 0.4596 3.0492	3.30 0.4596 3.0492	3.30 0.4596 3.0492 12.5383 0.2533
		1 4727	3 7848	0 8474	4 3108	0 040	35	1115.0	2 1574	7 2421	0.4911			1 760			330	3 32 0 4587	3 32 0.4587 3.0751 1	3 32 0.4587 3.0751 12.6028
1.74	0.6305	1.4873	3.3655	0.8389	4.3989	0.971	2.54	0.5092	2.1774	7.3602	0.4832	8.7851		1.789	1789 3.34	3.34	3.34 0.4578	3.34 0.4578 3.1011	3.34 0.4578 3.1011 12.8482	3.34 0.4578 3.1011 12.8482 0.2446
102010	0.6257	1.5019	3.4472	0.8302	4.4880	0.993	2.56	0.5074	2.1976	7.4792	0.4754	8.9161		1.808		3.36	3.36 0.4569	3.36 0.4569 3.1273	3.36 0.4569 3.1273 13.0045	3.36 0.4569 3.1273 13.0045 0.2404
512	0.6210	1.5167	3,5298	0.8215	4.5782	1.015	2.58	0.5056	2 2179	7 7200	0.4677	9.0482		1.827	1.827 3.38 1.846 3.40		3.38	3.38 0.4560	3.38 0.4560 3.1537	3.38 0.4560 3.1537 13.1618

							Table	B.2: NO	ormal si	nock wa	ve prope	Table B.2: Normal shock wave properties for $\gamma = 1.4$	$\gamma = 1.4$							
M1 M2		T_2/T_1	P2/P1	Poz/Pm	Pla/P1	$\Delta V/a_1$	MI	M2	T_2/T_1	P2/P1	Pte/Ptu	Pag/Ph	$\Delta V/a_1$	M ₁	M2	T_2/T_1	P_2/P_1	Paz/Pa	Poz/Pi	$\Delta V/a_1$
	-	.~	13.4791	0.2282	15.5297	2.606	4.22	0.4295	4.3994	20.6098	0.1154	23.3958	3.319	5.02	0.4149	5.8390	29.2338	809010	32.9115	4.017
			13.6392	0.2243	15.7062	2.624	424	0.4290	4.4324	20.8072	0.1135	23.6135	3.337	5.04	0.4147	5.8782	29.4685	865010	33.1705	4.035
3.46 0.4527		3.2607	13.8002	0.2205	15.8838	2.642	4.26	0.4286	4.4055	21.0055	0.1116	23.8324	3.354	90.u	0.4144	5.9175	29.7042	0.0589	33.4305	4.052
			14.1250	0.2129	16.2420	2.679	430	0.4277	4.5322	21.4050	0.1080	24.2731	3.390	5.10	0.4138	5.9966	30.1783	0.0572	33,9537	4.087
			Cardina Second	100	1	1	r.j		1	- and and	1	-		1	•	•				,
3.52 0.4504		3.3425	14.2888	0.2093	16,4227	2.697	4.32	0.4272	4.5658	21.6061	0.1062	24.4950	3.407	5.12	0.4136	6.0364	30.4168	0.0563	34.2169	4.104
			14.4535	0.2057	16,6044	2.715	4.34	0.4268	4.5995	21.8082	0.1045	24.7180	3.425	5.14	0.4133	6.0763	30.6562	0.0554	34.4810	4.121
			14.6192	0.2022	16.7871	2.733	4.36	0.4264	4.6334	22.0112	0.1028	24.9420	3.442	5.16	0.4130	6.1164	30.8965	0.0546	34.7462	4.139
			14.7858	0.1987	16.9708	2.751	4.38	0.4260	4.6675	22.2151	0.1011	25.1670	3.460	5.18	0.4128	6.1567	31.1378	0.0538	35.0125	4.156
3.60 0.4474		3.4537	14.9533	0.1953	17.1556	2.769	4.40	0.4255	4.7017	22.4200	666010	25.3930	3.477	5.20	0.4125	6.1971	31.3800	0.0530	35.2797	4.173
•		1	•			•			•		,				•	•	•	•	•	,
3.62 0.4467			15.1218	0.1920	17.3415	2.786	4.42	0.4251	4.7361	22.6258	0.0979	25.6201	3.495	5.22	0.4123	6.2376	31.6231	0.0522	35.5480	4.190
			15.2912	0.1887	17.5283	2.804	4.44	0.4247	4.7706	22.8325	0.0963	25.8482	3.512	5.24	0.4120	6.2784	31.8672	0.0514	35.8174	4.208
			15.4615	0.1855	17.7162	2.822	4.46	0.4243	4,8053	23.0402	2000	26.0773	3.530	5.26	0.4118	6.3192	32.1122	0.0506	36.0877	4.225
3.68 0.4446		3.56/4	15.6328	0.1823	17.9051	2.840	4.48	0.4239	4.8401	23.2488	0.0932	26.3075	3.547	5.28	0.4115	6.3603	32.3581	0.0499	36.3591	4.242
		1.1		10.00 M			,				10000 40		-	-	the state of the s	-	-	Area -		, [
(72 0.4433		3.6252	15.9781	0.1761	18,2860	2.876	4.52	0.4232	4.9102	23.6688	0.0902	26.7709	3.582	5.32	0.4110	6.4428	32.8528	0.0484	36.9050	4.277
			16.1522	0.1731	18.4781	2.894	4.54	0.4228	4.9455	23.8802	888010	27.0041	3.600	5.34	0.4108	6.4843	33.1015	0.0477	37.1794	4.294
	100		16.3272	0.1702	18.6711	2.912	4.56	0.4224	4.9810	24.0925	0.0874	27.2384	3.617	5.36	0.4106	6.5259	33.3512	0.0470	37.4550	4.311
3.78 0.4414		3.7130	16.5031	0.16/3	18.8652	2.930	4.58	0.4217	20233	24.3058	0.0846	27.4737	3,635	1 1 20	0.4103	1/19579	33,6018	0.0463	32.7315	4.328
3.82 0.4401			16.8578	0.1617	19.2564	2.965	4.62	0.4213	5.0882	24.7351	0.0832	27.9475	3.670	5.42	0.4099	6.6518	34.1058	0.0449	38.2877	4.363
3.84 0.4395		3.8022	17.0365	0.1589	19.4536	2983	4.64	0.4210	5.1243	24.9512	0.0819	28.1859	3.687	5.44	0.4096	6.6941	34.3592	0.0443	38.5673	4.380
3.86 0.4389			17.2162	0.1563	19.6518	3.001	4.66	0.4206	5.1605	25.1682	0.0806	28.4253	3.705	5.46	0.4094	6.7365	34.6135	0.0436	38.8479	4.397
3.90 0.4377		3.8928	17,5783	0.1510	20.0513	3.036	4.70	0.4199	5.2334	25.6050	0.0781	28.9073	3.739	5.50	0.4090	6.8218	35,1250	0.0424	39.4124	4.432
			L.	5.0	1	Aller	t	1	V	1	A.	-	a.j	¢	1	0	F	1.0	L'and	U
3.92 0.4372		3.9233	17.7608	0.1485	20.2526	3.054	4.72	0.4196	5.2701	25.8248	0.0769	29.1498	3.757	5.52	0.4088	6.8647	35.3821	0.0417	39.6961	4.449
			17.9442	0.1460	20.4549	3.072	4.74	0.4192	5.3070	26.0455	0.0756	29.3934	3.774	5.54	0.4085	6.9077	35.6402	0.0411	39.9809	4.466
3.96 0.4360			18.1285	0.1435	20.6583	3.090	4.76	0.4189	5.3440	26.2672	0.0745	29.6380	3.792	5.56	0.4083	6.9509	35.8992	0.0405	40.2667	4.483
4.00 0.4350		4.0469	18.5000	0.1388	21.0681	3.125	4.80	0.4183	5,4184	26.7133	0.0721	30,1303	3.826	5.60	0.4079	7.0378	36.4200	0.0394	40.8414	4.518
						9	į							1						1
			18.6871	0.1364	21.2745	3.143	4.82	0.4179	5.4009	26.9378	0.0710	30.3779	3.894	5.62	0.4077	7.0815	36.6818	865010	41.1303	epce.
4.04 0.4339		4.1096	10.0642	0.1342	21.4820	3.160	4.54	0.4173	5,6313	27.1632	0.0688	30.6267	3.861	10.0	0.4075	71403	2010/07	0.0377	41.4202	4.502
			10 2541	0 10 97	1000 10	418	4 88	04170	5 5400	276168	0.0677	31 1979	3 806	1 1 60	0 4071	70134	37 4738	0.0377	42 0032	4 587
			19.4450	0.1276	22.1106	3.213	4.90	0.4167	5.6073	27.8450	0.0667	31.3790	3.913	5.70	0.4069	7.2577	37.7383	0.0366	42.2962	4.604
			ĩ		1	r.	a.	ł				•		e.	ł	0	•	1	7	
		~	19.6368	0.1254	22.3223	3.231	4.92	0.4164	5.6455	28.0741	0.0657	31.6318	3.931	5.72	0.4067	7.3021	38.0048	0.0361	42.5903	4.621
			19.8295	0.1234	22.5349	3.249	4.94	0.4161	5.6839	28.3042	0.0647	31.8857	3.948	5.74	0.4065	7.3467	38 2722	0.0356	42.8854	4.638
		#1001#	N1412.52	0.1213	C/1485	A Diale	4.96		a man	and mana		AL DUE OF	- CANA	2.76		a state	and a state		43.1815	4.000
4.16 0.4309			2012100	0.1102	22.70 44	2 384	1 00	0.4158	5,7224	28.5352	0.0637	2705.62	2002	110	0.4063	7.3915	38.5405	0.0344	13 1796	1 677

			0.42.04
0.8071 0.5759	0.7135	1.2190	0.1579
	0.7198	1.2042	0.1506
0.8207 0.5960	0.7262	1.1899	0.1433
50	0.7328	1.1762	0.1361
	0.7397	1.1629	0.1288
320	0.7467	1.1501	0.1215
220	0.7540	11379	0.1142
2	1124 D	11111	2
27	0.7093	1.1149	1660'0
-	0.7773	1.1042	0.0926
	0.7856	1.0940	0.0855
100	0.7942	1.0842	0.0785
	0.8031	1.0750	0.0716
	,	,	1
	0.8123	1.0663	0.0648
	0.8218	1.0581	0.0582
	0.8316	1.0504	0.0517
201	0.8418	1.0432	0.0455
0.9247 0.7882	0.8524	1.0366	0.0394
	•	1	J
	0.8633	1.0304	0.0336
	0.8747	1.0248	0.0281
20	0.8865	1.0198	0.0230
	0.8988	1.0153	0.0182
0.9593 0.8745	0.9116	1.0113	0.0138
	-	-	1
212	0.0240	1 0070	0.000
	0.0207	1 0051	0.0044
	0.0001	10000	0.0020
	0.985/	1.0003	0.0005
1.0000 1.0000	1.0000	1.0000	0.0000
	1.0170	1.0003	0.0005
1.0132 1.0485	1.0348	1.0014	0.0021
1.0198 1.0743	1.0535	1.0031	0.0048
1.0263 1.1011	1.0730	1.0056	0.0089
	•	•	
	1.0934	1.0089	0:0145
	1.1148	1.0129	0.0218
	1.1373	1.0179	0.0310
	1.1609	1.0237	0.0423
1.0578 1.2542	1.1858	1.0305	0.0559
T/T* P/P*	0/q*	Po/Po*	4/L*/D
T/T [*] 1.0578 1.0578 1.0578 1.0578 1.0391 1.0391 1.0392		P/P* 1.2542 1.2542 1.2542 1.2542 1.2583 1.1583 1.1583 1.1583 1.1583 1.1583 1.10743 1.10743 1.07551 0.8561 0.7726 0.67552 0.6512 0.6065 - 0.5960	$\begin{array}{llllllllllllllllllllllllllllllllllll$

3.20	3.18	3.16	3.14	3.12	2	3.10	3.08	3.06	3.04	3.02		3.00	2.98	2.96	2.94	2.92		200	2.88	2.86	2.84	2.82		2.80	2.78	2.76	2.74	272	1	270	2.68	2.66	264	263		260	2 10	21	27	2 52	2.50	2.48	2.46	2.44	2.42	M
0.3937	0.3970	0.4004	0.4038	0.4072	4	0.4107	0.4142	0.4177	0.4213	0.4249	r	0.4286	0.4323	0.4360	0.4398	0.4436		0 4474	0.4513	0.4552	0.4592	0.4632		0.4673	0.4714	0.4755	0.4797	0.4839	ł	0.4882	0.4925	0.4969	0.5013	0 5057	and the	0.5102	0 5147	C012 0	05230	9862.0	0.5333	0.5381	0.5429	0.5478	0.5527	T/T*
0.1961	0.1981	0.2002	0.2024	0.2045	4	0.2067	0.2090	0.2112	0.2135	0.2158	1	0.2182	0.2206	0.2231	0.2256	0.2281	-	2002.0	0.2333	0.2359	0.2386	0.2414	+	0.2441	0.2470	0.2498	0.2528	0.2558	ł	0.2588	0.2619	0.2650	0.2682	0 7714		0 2747	0.7781	0 2815	0 2850	0 2885	0.2921	0.2958	0.2995	0.3033	0.3072	P/P*
0.4980	0.4991	0.5001	0.5012	0.5023	ł	0.5034	0.5045	0.5056	0.5068	0.5080	1	0.5092	0.5104	0.5116	0.5129	0.5142	-	2515.0	0.5169	0.5182	0.5196	0.5210	1	0.5225	0.5239	0.5254	0.5269	0.5285		0.5301	0.5317	0.5333	0.5350	0 5367	Concord (0 5385	0 5400	0 5401	05120	0 5458	0.5477	0.5497	0.5517	0.5537	0.5558	p/p*
5.1210	5.0248	4.9304	4.8377	4.7467	ł	4.6573	4.5696	4.4835	4.3989	4.3160	1	4.2346	4.1547	4.0763	3.9993	3.9238		3 8498	3.7771	3.7058	3.6359	3.5674	ł	3.5001	3.4342	3.3695	3.3061	3.2440		3.1830	3.1233	3.0647	3.0073	2 0511		2 8060	2 8420	7 7801	2 7272	2 6865	2.6367	2.5880	2.5403	2.4936	2.4479	P_0/P_0^*
0.5504	0.5478	0.5451	0.5424	0.5396		0.5368	0.5339	0.5310	0.5281	0.5252	i.	0.5222	0.5191	0.5160	0.5129	0.5097		05065	0.5033	0.5000	0.4966	0.4932	r.	0.4898	0.4863	0.4827	0.4791	0,4755	10	0.4718	0.4681	0.4643	0.4604	0 4565	and the second sec	0.4526	0.4486	0.4445	0.4404	04362	0.4320	0.4277	0.4233	0.4189	0.4144	4/L"/D
4	3.98	3.96	3.94	3.92		3.90	3.88	3.86	3.84	3.82		3.80	3.78	3.76	3.74	3.72		3 70	3.68	3.66	3.64	3.62		3.60	3.58	3.56	3.54	3.52		3.50	3	3.46	3.44	3 43		3 40	305	226	22	CE E .	3.30	ω L	3.26	3.24	30	M
			0.2923	92 0.2946		0 0.2969	88 0.2992	86 0.3015								72 0.3185						62 0.3314					54 0.3422	52 0.3450						0						0 3745	30 0.3776				22 0.3904	4 T/T*
							14																																		- 2					
			0.1372	0.1385	1		0.1410	0.1423								0.1517						0.1590					0.1653	0.1669						3						01843	0.1862				0.1940	P/P"
0.4677	0.4683	0.4688	0.4694	0.4700	9	0.4706	0.4712	0.4718	0.4724	0.4730	ŧ.	0.4737	0.4743	0.4750	0.4757	0.4763	-	0.4770	0.4777	0.4784	0.4791	0.4799	r	0.4806	0.4813	0.4821	0.4829	0.4837	•	0.4845	0.4853	0.4861	0.4869	0.4878		0.4896	0.4805	04904	04013	0.4922	0.4931	0.4941	0.4951	0.4960	0.4970	p/p-
10.7188	10.5289	10.3420	10.1581	9.9771	1	9.7990	9.6237	9.4513	9.2817	9.1148	7	8.9506	8.7891	8.6302	8.4739	8.3202		8 1601	8.0204	7.8742	7.7305	7.5891	7	7.4501	7.3135	7.1791	7.0471	6.9172	ŀ	6.7896	6.6642	6.5409	6.4198	2001F 9	Contraction of the	61837	60687	A OURS	58448	57358	5.6286	5.5234	5.4201	5.3186	5.2189	P_0/P_0^*
0.6331	0.6315	0.6298	0.6282	0.6265	4	0.6248	0.6231	0.6214	0.6197	0.6179	7	0.6161	0.6143	0.6125	0.6106	0.6087	-	0.6068	0.6049	0.6030	0.6010	0.5990	L.	0.5970	0.5949	0.5928	0.5907	0.5886	1	0.5864	0.5842	0.5820	0.5798	0 5775	No.	0 5752	0.5720	0 5705	0 5481	0 5657	0.5632	0.5607	0.5582	0.5557	0.5531	4/L"/D
	+	*					*	+	+				*	+		+			*		*					*	+	*		1			•		2		10						-		-	-
				4.72	4																								•												4.10					
0.2140	0.2155	0.2169	0.2184	0.2200	ł	0.2215	0.2230	0.2246	0.2262	0.2278	N.	0.2294	0.2310	0.2326	0.2343	0.2359		0 2376	0.2393	0.2410	0.2428	0.2445	1	0.2463	0.2481	0.2499	0.2517	0.2536	•	0.2554	0.2573	0.2592	0.2611	1596.0	1	02650	0.2620	00600	0.9710	02730	0.2751	0.2772	0.2793	0.2814	0.2835	T/T*
0.0964	0.0971	0.0979	0.0986	0.0994	2	0.1001	0.1009	0.1017	0.1025	0.1033		0.1041	0.1049	0.1058	0.1066	0.1075	-	0 1083	0.1092	0.1101	0.1110	0.1119	1	0.1128	0.1137	0.1147	0.1156	0.1166		0.1175	0.1185	0.1195	0.1205	0.1215		0.1226	01235	01247	01257	0.1268	0.1279	0.1290	0.1302	0.1313	0.1325	P/P=
0.4504	0.4507	0.4510	0.4514	0.4517	a	0.4521	0.4525	0.4528	0.4532	0.4536		0.4539	0.4543	0.4547	0.4551	0.4555	-	0.4550	0.4563	0.4567	0.4571	0.4575	1	0.4579	0.4584	0.4588	0.4592	0.4597		0.4601	0.4606	0.4611	0.4615	0.4620		0.4625	0.4630	0.4635	0.4640	0.4645	0.4650	0.4655	0.4661	0.4666	0.4672	P/P*
21 2637	20.9179	20.5770	20.2409	19.9095	1	19.5828	19.2608	18.9433	18.6303	18.3218	7	18.0178	17.7181	17.4228	17.1317	16.8449		16 5600	16.2837	16.0092	15.7388	15.4724	1	15.2099	14.9513	14.6965	14.4456	14.1984	ł	13.9549	13.7151	13.4789	13.2463	13 0172	and and	12 7016	13 5605	12 1508	12 1354	11 9234	11.7147	11.5091	11.3068	11.1077	10.9117	P_0/P_0^*
0.6842	0.6831	0.6821	0.6811	0.6800	9	0.6790	0.6779	0.6768	0.6757	0.6746	Ŧ	0.6734	0.6723	0.6712	0.6700	0.6688	-	0.6676	0.6664	0.6652	0.6640	0.6627	-	0.6615	0.6602	0.6589	0.6576	0.6563		0.6550	0.6536	0.6523	0.6509	0.6405	Sector 1	0.6481	0.6467	0.6450	0 6438	0.6423	0.6408	0.6393	0.6378	0.6362	0.6346	4ft"/D

Table D.2: Fanno flow properties for $\gamma = 1.4$

0.80		1.14			-			7772	0.62 0.							1					13						0.32 0	0.30 0.				0.22 0.			0.18 0.			12			0.02 0.0			M I
.0255			1.0026		0.9929			0.9530	0.9358		0.9167				0.8196					0.6903 1							0.4512	U.AUSY				0.2445						762070		0.0560				1/1-
1.2658	00/1	1.3585	1.3907	o!	1.4235	1.4569	1.4908	1.5253	1.5603	t	1.5957	1.6316	1.6678	1.7043	1.7409	2	1.7778	1.8147	1.8515	1.8882	1.9247	1	1.9608	1.9964	2.0314	0,0647	0001	2.1314	2.1626	2.1925	2.2209	2.2477	N)	2.2727	2 2959	2 3170	2 3350	2.3526		23669	2 3797	1 9000	2.3987	-3/4
1.2344	1.3047	1.3442	1.3871	1	1.4337	1.4844	1.5399	1.6006	1.6673	ŀ	1.7407	1.8219	1.9120	2.0122	2.1243	y.	2.2500	2.3918	2.5525	2.7355	2.9454		3.1875	3.4688	3,7984	41877	16573	0.2130	5.8980	6.7470	7.8171	9.1921		11 0000	13.4434	16 8594	21.8418	29.5185	-	42.2500	110.3241	112 3011	1042.2500	-010°
0.9639	CCP42.0	0.9344	0.9221		0.9085	0.8935	0.8771	0.8592	0.8398		0.8189	0.7965	0.7725	0.7470	0.7199		0.6914	0.6614	0.6301	0.5975	0.5638	1	0.5290	0.4935	0.4572	0.420%	0 3837	0.5469	0.3104	0.2745	0.2395	0.2057	No. of Concession, Name	0 1736	0.1432	0 1151	0 0895	0.0666	-	0.0468	0.0202	0/00/0	0.0019	T0/10
1.0193	1.0270	1.0325	1.0376	3	1.0431	1.0489	1.0550	1.0615	1.0682	r,	1.0753	1.0826	1.0901	1.0979	1.1059	3	1.1141	1.1224	1.1308	1.1394	1.1480	a.	1.1566	1.1652	1 1737	1 1822	1 1004	1.1985	1.2064	1.2140	1.2213	1.2281		1 2346	1 2406	1 2461	1 2510	1.2554		1.2591	1 7672	1.2000	1.2675	P0/P0
1.60	1.30	1.54	1.52	,	1.50	1.48	1.46	1.44	1.42	e	1.40	1.38	1.36	1.34	1.32	4	1.30	1.28	1.26	1.24	1.22	r.	1.20	118	116	114	113	1.10	1.08	1.06	1.04	1.02	1	100	86.0	0.95	0.94	0.92	-	0.90	00.0	0.02	0.82	M
0.7017	11221	07319	0.7422		0.7525	0.7629	0.7735	0.7840	0.7947	ĩ	0.8054	0.8161	0.8269	0.8377	0.8484		0.8592	0.8699	0.8805	0.8911	0.9015	1	0.9118	0.9220	0.9320	0 9417	0.0510	0.9603	0.9691	0.9776	0.9855	0.9930	1	1.0000	1.0064	1.0121	1 0170	1.0212		1.0245	1.0260	1.0285	1.0276	1/1-
0.5236	OPPC.U	0.5555	0.5668	ï	0.5783	0.5902	0:6024	0.6149	0.6278	4	0.6410	0.6546	0.6686	0.6830	0.6978	9	0.7130	0.7287	0.7447	0.7613	0.7783	1	0.7958	0.8137	0.8322	0.8517	0.8708	0.8909	0.9115	0.9327	0.9546	0.9770	-	1.0000	1.0236	10479	1 0728	1.0984		1.1246	1.1/91	1.20/3	1.2362	Al.A
0.7461	CHC/TO	0.7590	0.7637	•	0.7685	0.7736	0.7788	0.7843	0.7900	۲	0.7959	0.8021	0.8086	0.8154	0.8225	•	0.8299	0.8376	0.8458	0.8543	0.8633		0.8727	0.8826	066870	00000	0.0155	0.927	0.9406	0.9542	0.9686	0.9838		1.0000	1.0172	10354	1 0549	1.0756		1.0977	1 12140/	1.1/38	1.2030	610-
0.8842	796010	0.0015	0.9042	•	0.9093	0.9143	0.9193	0.9243	0.9293		0.9343	0.9391	0.9440	0.9487	0.9534	•	0.9580	0.9624	0.9668	0.9709	0.9749	Į.	0.9787	0.9823	0.9856	0.0887	0.0015	606600	09960	0.9977	686670	0.9997	No. of the second	1.0000	76660	8800.0	0.0073	0.9951		0.9921	0.0420	18/60	0.9715	10/10
1.1756	77511	1.1419	1.1315	1	1.1215	1.1120	1.1028	1.0940	1.0856	ł	1.0777	1.0701	1.0629	1.0561	1.0497	at.	1.0437	1.0380	1.0328	1.0279	1.0235		1.0194	1.0157	1.0124	10005	1 0070	1.0042	1.0031	1.0017	1,0008	1.0002	No.	1.0000	1.0002	10008	1 0017	1.0031	-	1.0049	1 0000	1.0128	1.0157	P0/P0
2.40	200	2.34	2.32	4	2.30	2.28	2.26	2.24	2.22	1	2.20	2.18	2.16	2.14	2.12	3	2.10	2.08	2.06	2.04	2.02	s.	2.00	1.98	1.96	1 04	1 .	1.90	1.88	1.86	1.84	1.82	1	180	178	176	1 74	1.72	,	1.70	1 42	1.04	1.62	M
0.4038	CEIECO	0.4200	0.4256	4	0.4312	0.4370	0.4428	0.4488	0.4549	r	0.4611	0.4673	0.4737	0.4802	0.4868	ä	0.4936	0.5004	0.5074	0.5144	0.5216		0.5289	0.5364	0.5439	0 5516	1055 0	0.5673	0.5754	0.5836	0.5919	0.6004	-	6809.0	0.6176	0 6265	0.6355	0.6445	-	10000	0.4421	279910	0.6919	1/1-
0.2648	02/20	0.2769	0.2812	1	0.2855	0.2899	0.2945	0.2991	0.3038	1	0.3086	0.3136	0.3186	0.3238	0.3291	4	0.3345	0.3401	0.3458	0.3516	0.3575	7	0.3636	0.3699	0.3763	8686 0	0 3805	0.3964	0.4035	0.4107	0.4181	0.4257	-	0.4335	0.4415	0.4497	0.4581	0.4668		0.4756	0.4940	O ADA	0.5135	-414
0.6557	10001	0.000	0.6607		0.6621	0.6635	0.6649	0.6664	0.6679		0.6694	0.6710	0.6726	0.6743	0.6760		0.6778	0.6796				ł	0.6875	0.6896	0.6918	0.6940	0 6064	U.bygg	0.7012	0.7038	0.7064	0.7091		07119	0.7148	07178	0.7210	0.7242		0.7275	012210	0.7365	0.7421	6/9
14			P		07	0.7428	0.7460	0.7493	0.7527	1	0.7561	0.7596	0.7631	0.7667	0.7704	ě	0.7741	0.7778	0.7816	0.7855	0.7894	0	0.7934	0.7974	0.8015	0.8057	0 90000	0.8141	0.8185	0.8228	0.8273	0.8317		0.8363	0.8409	0 8455	0.8502	0.8549		0.8597	10.9645	CB/80	0.8792	10/10
0.7242	2007-0	0.7333	0.7364	•	0.7395	428	5	93	13		19	8	22	1	÷															1.000		1.1			~		(T) (1)	~		1.2.12				

3.20	3.18	3.16	3.14	3.12	i)	3.10	308	3.06	3.04	3.02	3.00	2.98	2.96	2.94	2.92	•	2.90	2.88	2.86	2.84	2.82		2.80	2.78	2.76	2.74	2.72	2.70	2.68	2.66	2.64	2.62	.]	2.60	2 58	2.56	254	2.52		2.50	2.48	2.46	2.44	M
0.2508	0.2535	0.2563	0.2592	0.2620	1	0.2650	07670	0.2709	0.2740	0.2771	0.2803	0.2835	0.2868	0.2901	0.2934		0.2969	0.3004	0.3039	0.3075	0.3111		0.3149	0.3186	0.3225	0.3264	0.3304	0.3344	0.3385	0.3427	0.3469	0.3512	Concession of the	0.3556	0.3601	0.3646	0.3692	0.3739	1	0.3787	0.3836	0.3885	0.3935	1/1
0 1565	0.1583	0.1602	0.1621	0.1641		0.1660	01681	0.1701	0.1722	0.1743	0.1765	0.1787	6081.0	0.1832	0.1855		0.1879	0.1903	0.1927	0.1953	0.1978		0.2004	0.2030	0.2058	0.2085	0.2113	0.2142	0.2171	0.2201	0.2231	0.2262	.]	0.2294	0.2326	0.2359	0.2392	0.2427	0	0.2462	0.2497	0.2534	0.2571	Ala
06740	0.6245	0.6251	0.6256	0.6261	,	0.6267	66773	0.6278	0.6284	0.6290	0.6296	0.6303	606309	0.6315	0.6322		0.6329	0.6336	0.6343	0.6350	0.6357	ï.	0.6365	0.6372	0.6380	0.6388	0.6397	0.6405	0.6413	0.6422	0.6431	0.6440		0.6450	0.6459	0.6469	0.6479	0.6489	1	0.6500	0.6511	0.6522	0.6533	did
105270	0.6386	0.6402	0.6418	0.6435		0.6452	0.6469	0.6486	0.6504	0.6522	0.6540	866910	0.6577	960970	0.6615		0.6635	0.6655	0.6675	0.6696	0.6717	7	0.6738	0.6760	0.6781	0.6804	0.6826	0.6849	0.6873	0.6896	0.6921	0.6945	-	0.6970	2669.0	0.7021	0.7047	0.7074		0.7101	0.7128	0.7156	0.7184	10/10
4.0871	4.0154	3.9449	3.8756	3.8076	ŀ	3.7408	3 6753	3.6108	3.5476	3.4854	3.4245	3.3646	3.3058	3.2481	3.1914		3.1359	3.0813	3.0278	2.9752	2.9237	1	2.8731	2.8235	2.7748	2.7270	2.6802	2.6343	2.5892	2.5451	2.5018	2.4593	1	2.4177	2 3770	2.3370	2.2978	2.2594		2.2218	2.1850	21489	2.1136	0/1/01
	3.98	3.96	3.94	3.92						3.82		3.78						3.68		3.64	3.62	¥.		3.58		3.54	3.52	3.50				3.42						3.32	2	3.30			3.24	
4.00	3.98	3.96	3.94	3.92	ý.	3.90	288	3.86	3.84	3.82	3.80	3.78	3.76	3.74	3.72		3.70	3.68	3.66	3.64	3.62	¥.	3.60	3.58	3.56	3.54	3.52	3.50	3.48	3.46	3.44	3.42		3.40	3 38	3.36	3.34	3.32	į.	3.30	3.28	3.26	3.24	M
	0.1699 (0.1714 (0.1730 (0.1746 (_				0.1830 (0.1848 (0.1939 (0.1977 (0.1997 (0.2017 (T.	0.2037 (0.2099 (0.2120 (0.2142 (0.2209 0	0.2232 (-	0.2352 0					0.2454 (
0.1006	0.1036	0.1046	0.1056	0.1066		0.1077	01087	0.1098	0.1109	0.1120	0.1131	0.1143	0.1154	0.1166	0.1178	,	0.1190	0.1202	0.1215	0.1228	0.1241	1	0.1254	0.1267	0.1280	0.1294	0.1308	0.1322	0.1337	0.1351	0.1366	0.1381	1 and a second	0.1397	0.1412	0.1428	0.1444	0.1461	1	0.1477	0.1494	0.1511	0.1529	114
2	0	0.6	0.6	0.6		0.6	0,6	0.6113	0.6116	0.6119	0.6122	0.6125	0.6128	0.6131	0.6134		0.6138	0.6141	0.6144	0.6148	0.6151		0.6155	0.6158	0.6162	0.6166	0.6170	0.6173	0.6177	0.6181	0.6185	0.6190		0.6194	0.6198	0.6202	0.6207	0.6211		0.6216	0.6221	0.6225	0.6230	
LOU .	0.6096	0.6099	0.6102	0.6104	1	0.6107	06110	13	16	19	B	13	1 Se	12	E.		00	-									-								-		~	-		6	2	ы	83	
	6096 0.5900	099 0.5909	5102 0.5918	104 0.5928						19 0.5977	22 0.5987						0.6040		0.6062	0.6074	0.6085		0.6097			0.6133	0.6145	0.6158	0.6171			0.6210	-	0.6224			2	1 0.6280					90 0.6339 90 0.6	0/0

Table E.2: Rayleigh flow properties for $\gamma = 1.4$

448 440 $\begin{array}{r} 4.52\\ 4.54\\ 4.54\\ 4.54\\ 4.56\\ 4.58\\$ 4.22 4.24 4.26 4.28 4.02 4.04 4.06 4.08 M 0.1238 0.1229 0.1219 0.1209 0.1209 0.1289 0.1279 0.1268 0.1258 0.1258 0.1248 0.1343 0.1332 0.1321 0.1321 0.1300 0.1400 0.1388 0.1377 0.1365 0.1354 0.1461 0.1448 0.1436 0.1424 0.1412 0.1525 0.1512 0.1499 0.1486 0.1473 0.1539 0.1580 0.1566 0.1552 0.1668 0.1653 0.1638 0.1623 0.1609 0.1594 T/T* 1 0.0960 0.0951 0.0951 0.0934 0.0947 0.0909 0.0890 0.0885 0.08777 0.08777 0.07777 0.0775 0.1016 0.1006 0.0997 0.0987 0.0978 0.0969 P/P* 1 - 9 0.6075 0.6077 0.6077 0.6067 0.6067 0.6067 0.6065 0.6065 0.6065 0.6057 0.605 0.6091 0.6089 0.6086 0.6084 0.6081 p/p 0.5839 0.5831 0.5823 0.5814 0.5873 0.5864 0.5856 0.5847 0.5807 0.5799 0.5779 0.5776 0.5776 0.5776 0.5776 0.5776 0.5776 0.5772 0.5776 0.5772 0.5776 0.5772 0.5776 0.5772 0.5772 0.5775 0.5775 0.5775 0.5775 0.5776 0.5776 0.5776 0.5776 0.5776 0.5776 0.5776 0.5776 0.5667 0.5666 0.55664 0.55642 0.55665662 0.55666566566666566666666666666666 0.5882 To/To 10.7766 10.9572 11.1406 11.3267 11.5155 11.7072 11.9016 12.0989 12.2991 12.5023 9.9125 10.0802 10.2504 10.4232 10.5985 14.9393 15.1802 15.4245 15.6722 15.9234 -13.7843 14.0088 14.2365 14.4675 14.7017 12.7083 12.9174 13.1295 13.3446 13.5629 9.1110 9.2665 9.4243 9.5846 9.7473 8.5125 8.6587 8.8072 8.9579 8.3686 P_0/P_0^* 1 1 . .