| Name: <br> Enrolment No: |  |  |  |
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| UNIVERSITY OF PETROLEUM AND ENERGY STUDIES   <br>  End Semester Examination, MAY 2021  <br> Course: Pipeline Transportation of Oil and Gas Semester: VIII  <br> Program: B. Tech. Chemical Engineering Time 03 hrs.  <br> Course Code: CHGS3007P Max. Marks: 100  <br> Instructions: Attempt All Questions   |  |  |  |
| SECTION A |  |  |  |
| S. No. | ATTEMPT ALL QUESTIONS- APPENDIX ON PAGE NO. 5-7 (5*6=30 MARKS) | Marks | CO |
| Q. 1 | Illustrate the term 'Erosional Velocity' in pipelines | 5 | CO1 |
| Q. 2 | Explain the methodology adopted to calculate the 'Number of Pumps' required to transport oil. | 5 | CO4 |
| Q. 3 | Discuss 'Line Pack Volume'. | 5 | CO1 |
| Q. 4 | Discuss the difference between Reciprocating pumps and Centrifugal pumps with their limitations. | 5 | CO3 |
| Q. 5 | Discuss the term 'MAOP' in oil and gas pipelines | 5 | CO2 |
| Q. 6 | Explain the difference between NPSHA and NPSHR | 5 | CO4 |
| SECTION B(ATTEMPT ALL QUESTIONS) |  |  |  |
| Q. 7 | Explain the purpose and types of PIGS used in the pipeline industry. | 10 | CO2 |
| Q. 8 | Explain performance curves for centrifugal pumps | 10 | CO5 |
| Q. 9 | (a) Illustrate the term 'Class location in compressors'. <br> (b) Explain the specific speed of pumps. | 10 | CO4 |
| Q. 10 | If the total pressure required to pump the liquid is 2000 psi and the suction pressure of each pump is 50 psi , then calculate the number of pumping stations required with 1050-psi discharge pressure. | 10 | CO3 |
| Q. 11 | Explain in short the pipeline construction activities | 10 | CO2 |

## SECTION-C <br> (ATTEMPT ANY ONE QUESTION) MISSING DATA ARE TO BE SUITABLY ASSUMED

| Q. 12 | The Salaya - Mathura pipeline is used for transporting oil from Salaya to Mathura refinery. There are two intermediate stations, one at Viramgram and the other one at Koyli. The length of Salaya- Mathura pipeline is 48 miles and is of 18 inch in diameter, with 0.281 inch wall thickness. It is constructed of 5LX-65 grade steel. At origin station Salaya, crude oil of specific gravity 0.85 and 10 cSt viscosity enters the pipeline at a flow rate of $6000 \mathrm{bbl} . / \mathrm{hr}$. At first intermediate station Viramgram (milepost 22) a new stream of crude oil with a specific gravity of 0.82 and 3.5 cSt viscosity enters the pipeline at a flow rate of 1000 bbl ./hour. The mixed stream then continues to another intermediate station Koyli (milepost 32) where 3000 bbl. / hour is stripped off the pipeline. The remaining volume continues to the end of the pipeline at delivery station Mathura. <br> (a) Evaluate the pressure required at origin station Salaya and the composition of the crude oil arriving at terminus Mathura at a minimum delivery pressure of 50 psi . Assume elevations at Salaya, Viramgram, Koyli, and Mathura to be 100, 150, 250, and 300 feet, respectively. Use the Modified Colebrook-White equation for pressure drop calculations and assume a pipe roughness of 0.002 inches. <br> (b) Evaluate the pump HP that will be required at Salaya to maintain this flow rate, assuming 50-psi pump suction pressure at Salaya and $80 \%$ pump efficiency? <br> (c) If a positive displacement (PD) pump is used to inject the stream at Viramgram, solve for pressure and HP are required at Viramgram? | 20 | CO5 |
| :---: | :---: | :---: | :---: |
| Q13 | A natural gas pipeline, 140 miles long from Dover to Leeds, is constructed of NPS 16, 0.250 in. wall thickness pipe, with an MOP of 1200 psig . The gas specific gravity and viscosity are 0.6 and $8 \times 10^{-6} \mathrm{lb} / \mathrm{ft}-\mathrm{s}$, respectively. The pipe roughness can be assumed to be $700 \mu \mathrm{in}$. and the base pressure and base temperature are 14.7 psia and $60^{\circ} \mathrm{F}$, | 20 | CO 3 |


|  | respectively. The gas flow rate is 175 MMSCFD at $80^{\circ} \mathrm{F}$, and the delivery pressure <br> required at Leeds is 800 psig. <br> a) Evaluate the pressure required at inlet to deliver the gas at Leeds? <br> b) Analyze, if the gas can be delivered at the calculated inlet pressure from Dover? If <br> not, mention the reasons. <br> c) Assuming if only one intermediate compressor is installed at the mid-point of the <br> pipeline at Kent, will it be able to deliver the gas at Leeds at delivery pressure. Mention <br> reasons. <br> d) If not, calculate the exact location of the compressor. Also, for this location, <br> calculate the suction pressure and compression ratio at Kent. <br> Assume $Z=0.85$ |  |
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## APPENDIX

## All Notations have their usual meaning and units

## 1. Frictional Pressure drop equation in oil pipelines

$$
\mathrm{Pm}=0.0605 \mathrm{fQ}^{2}\left(\mathrm{Sg} / \mathrm{D}^{5}\right)
$$

## 2. Pressure drop equation for gas pipelines

$$
Q=77.54\left(\frac{T_{b}}{P_{b}}\right)\left(\frac{P_{1}^{2}-P_{2}^{2}}{G T_{f} L Z f}\right)^{0.5} D^{2.5}
$$

## 3. Reynolds Equation for Gas Pipelines

$\operatorname{Re}=0.5134\left(\frac{P_{b}}{T_{b}}\right)\left(\frac{G Q}{\mu D}\right)$

$$
\begin{equation*}
\operatorname{Re}=0.0004778\left(\frac{P_{b}}{T_{b}}\right)\left(\frac{G Q}{\mu D}\right) \tag{USCS}
\end{equation*}
$$

4. Reynolds No. for Crude Oil Pipelines
a) $\mathrm{R}=92.24 \mathrm{Q} /(\mathrm{v}$ D)

Where: $\mathrm{Q}=$ Flow rate, $\mathrm{bbl} /$ day; $\mathrm{D}=$ Internal diameter, in.; $v=$ Kinematic viscosity, cSt
b) $\mathbf{R}=\mathbf{3 5 3 , 6 7 8} \mathbf{Q} /(\mathbf{v D})$

Where: $\mathrm{Q}=$ Flow rate, $\mathrm{m}^{3} / \mathrm{hr}$.; $\mathrm{D}=$ Internal diameter, $\mathrm{mm} ; ~ v=$ Kinematic viscosity, cSt $\mathrm{D}=$ Pipe internal diameter, in.

## 5. Modified Colebrook White Equation

$$
\frac{1}{\sqrt{f}}=-2 \log _{10}\left(\frac{e}{3.7 D}+\frac{2.825}{\operatorname{Re} \sqrt{f}}\right)
$$

## 6. Coversion Equations for SSU to Centistokes

$$
\begin{array}{lc}
\text { Centistokes }=0.226(S S U)-\frac{195}{S S U} & 32 \leq S S U \leq 100 \\
\text { Centistokes }=0.220(S S U)-\frac{135}{S S U} & S S U \succ 100
\end{array}
$$

7. Horsepower required to compress gas in compressor

$$
H P=0.0857\left(\frac{\gamma}{\gamma-1}\right) Q T_{1}\left(\frac{Z_{1}+Z_{2}}{2}\right)\left(\frac{1}{\eta_{a}}\right)\left[\left(\frac{P_{2}}{P_{1}}\right)^{\frac{\gamma-1}{\gamma}}-1\right]
$$

## 8. Adiabatic Efficiency of Compressor

$$
\eta_{a}=\left(\frac{T_{1}}{T_{2}-T_{1}}\right)\left[\left(\frac{z_{1}}{z_{2}}\right)\left(\frac{P_{2}}{P_{1}}\right)^{\frac{\gamma-1}{\gamma}}-1\right]
$$

9. BHP required to pump the liquid

$$
B H P=\frac{Q P}{2449 E}
$$

$\mathbf{Q}=$ flow rate (barrel per hr.) $\quad \mathbf{P}=$ Differentia pressure (psi)
10. Equivalent diameter equation

$$
D_{e}=D_{1}\left[\left(\frac{1+\text { Const }}{\text { Const }}\right)^{2}\right]^{1 / 5} \quad \text { Const }=\sqrt{\left(\frac{D_{1}}{D_{2}}\right)^{5}\left(\frac{L_{2}}{L_{1}}\right)}
$$

11. Head to pressure conversion:

$$
\text { Head }=\frac{2.31 p s i g}{G}(U S C S)
$$

## 12. Specific gravity of blended liquids

$$
S_{b}=\frac{Q_{1} S_{1}+Q_{2} S_{2}+\ldots \ldots Q_{n} S_{n}}{Q_{1}+Q_{2}+\ldots . Q_{n}}
$$

13. Viscosity of blended liquids

$$
\sqrt{v_{b}}=\frac{Q_{1}+Q_{2}+Q_{3} \ldots .}{\left(\frac{Q_{1}}{\sqrt{v_{1}}}+\frac{Q_{2}}{\sqrt{v_{2}}}+\frac{Q_{3}}{\sqrt{v_{3}}} \cdots . .\right)}
$$

