| Name: <br> Enrolment No: |  |  |  |
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| Cours <br> Progr <br> Cours <br> Instru <br> where | UNIVERSITY OF PETROLEUM AND ENERGY STUDIES  <br> Special Examination, January 2021  |  | grams, |
| SECTION - A ( $6 \times 5=30$ marks) <br> (Answer all the questions) |  |  |  |
| S. No. |  | Marks | CO |
| 1. | A rigid vessel, containing three moles of nitrogen gas at $30^{0} \mathrm{C}$ is heated to $250{ }^{\circ} \mathrm{C}$. Assume that the average heat capacity of nitrogen to be $\mathrm{C}_{\mathrm{p}}=29.1 \mathrm{~J} / \mathrm{mol}-\mathrm{K}$ and $\mathrm{C}_{\mathrm{v}}=$ $20.8 \mathrm{~J} / \mathrm{mol}-\mathrm{K}$. The heat required, neglecting the heat capacity of the vessel, is <br> (a) 13728 J <br> (b) 19206 J <br> (c) 4576 J <br> (d) 12712 J | 5 | CO1 |
| 2. | Keeping the pressure constant, to double the volume of a given mass of an ideal gas at $27^{\circ} \mathrm{C}$, the temperature should be raised to <br> (a) $270{ }^{\circ} \mathrm{C}$ <br> (b) $327^{\circ} \mathrm{C}$ <br> (c) $300^{\circ} \mathrm{C}$ <br> (d) $540{ }^{\circ} \mathrm{C}$ | 5 | CO2 |
| 3. | The compressibility factor for steam at 523.15 K and 1800 kPa using the truncated virial equation, with the value of $B$ from generalized Pitzer correlations, is $\qquad$ Virial coefficients $B^{0}$ and $B^{1}$ are: $B^{0}=0.083-\frac{0.422}{T_{r}^{1.6}} \text { and } B^{1}=0.139-\frac{0.172}{T_{r}^{4.2}}$ <br> For steam: $\mathrm{T}_{\mathrm{c}}=647.1 \mathrm{~K}, \mathrm{P}_{\mathrm{c}}=220.55$ bar and $\omega=0.345$. <br> (a) 1 <br> (b) 0.975 <br> (c) 0.938 <br> (d) 0.905 | 5 | CO3 |


| 4. | The degree of freedom for a two phase vapor-liquid system comprised of chloroform, 1,4-dioxane and ethanol <br> (a) 1 <br> (b) 2 <br> (c) 3 <br> (d) 4 |  |  |  | 5 | CO4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5. | The vapor pressures of benzene and toluene are 3 atm and $4 / 3 \mathrm{~atm}$, respectively. A liquid feed of 0.4 mol benzene and 0.6 mol toluene is vaporized. Assuming that the products are in equilibrium, the vapor phase mole fraction of benzene is <br> (a) 0.2 <br> (b) 0.4 <br> (c) 0.6 <br> (d) 0.8 |  |  |  | 5 | CO4 |
| 6. | A Carnot refrigeration cycle absorbs heat at $3{ }^{\circ} \mathrm{C}$ and rejects heat at $27^{\circ} \mathrm{C}$. Calculate the coefficient of performance. <br> (a) 0.125 <br> (b) 1.125 <br> (c) 11.5 <br> (d) 12.5 |  |  |  | 5 | $\mathrm{CO5}$ |
| SECTION - B ( $5 \times 10=50$ marks) <br> (Answer all the questions) |  |  |  |  |  |  |
| S. No. |  |  |  |  | Marks | CO |
| 1. | One mole of gas the data given quantities: | ystem un g table to | r step th Q (J) $?$ -3800 -800 $?$ $?$ | s cycle. Use r the missing | 10 | CO1 |

\begin{tabular}{|c|c|c|c|}
\hline 2. \& Determine the expressions for \(\mathrm{G}^{\mathrm{R}}\) and \(\mathrm{H}^{\mathrm{R}}\) implied by the three-term virial equation in volume. \& 10 \& \(\mathrm{CO3}\) \\
\hline 3. \& \begin{tabular}{l}
The molar volume \(\left(\mathrm{cm}^{3} / \mathrm{mol}\right)\) of a binary liquid mixture at T and P is given by
\[
V=120 x_{1}+70 x_{2}+\left(15 x_{1}+8 x_{2}\right) x_{1} x_{2}
\] \\
Find expressions for partial molar volumes of species 1 and 2 . Show that these expressions satisfy Gibbs/Duhem equation.
\end{tabular} \& 10 \& CO 3 \\
\hline 4. \& \begin{tabular}{l}
A Carnot refrigerator has tetrafluoroethane as the working fluid. For \(\mathrm{T}_{\mathrm{C}}=261.15 \mathrm{~K}\) and \(\mathrm{T}_{\mathrm{H}}=311.15 \mathrm{~K}\), determine \\
(a) the heat addition per kg of fluid \\
(b) the heat rejection per kg of fluid \\
(c) the mechanical power per kg of fluid for each of the four steps \\
(d) the coefficient of performance \(\omega\) for the cycle \\
Thermodynamic properties of Saturated tetrafluoroethane are given in Table 1.
\end{tabular} \& 10 \& CO4 \\
\hline 5. \& A vapor mixture of \(20 \mathrm{~mol} \%\) methane, \(30 \mathrm{~mol} \%\) ethane and \(50 \mathrm{~mol} \%\) propane are available at \(30{ }^{\circ} \mathrm{C}\). Making use of the K factors, determine the pressure at which the condensation begins if the mixture is isothermally compressed. Also, estimate the composition of the first drop of liquid that forms. \& 10 \& CO5 \\
\hline \multicolumn{4}{|c|}{\begin{tabular}{l}
SECTION - C ( \(\mathbf{1 \times 2 0}=\mathbf{2 0}\) marks \()\) \\
(Answer all the questions)
\end{tabular}} \\
\hline 1.(a)

(b) \& | An inventor has devised a complicated non-flow process in which 1 mol of air is the working fluid. The net effects of the process are claimed to be: |
| :--- |
| - A change in state of air from 523.15 K and 3 bar to 353.15 K and 1 bar |
| - A production of 1800 J of work |
| - The transfer of an undisclosed amount of heat to a heat reservoir at 303.15 K Determine whether the claimed performance of the process is consistent with the second law. Assume that air is an ideal gas for which $C_{p}=(7 / 2) R$. |
| An ideal gas, $C_{p}=(7 / 2) R$, is heated in a steady-flow heat exchanger from 343.15 K to 463.15 K by another stream of the same ideal gas which enters at 593.15 K. The flow rates of the two streams are the same and heat losses from the exchanger are negligible. | \& 10 \& CO 2 \\

\hline
\end{tabular}

|  | (i) Calculate the molar entropy change of the two gas streams for counter current flow <br> in the exchanger? <br> (ii) Calculate the total entropy change? |  |  |
| :--- | :--- | :--- | :--- |

Table: 1 Thermodynamic properties of Saturated Tetrafluoroethane

| Temperature <br> $(\mathrm{K})$ | Saturation <br> pressure <br> MPa | Liquid <br> density <br> $\mathrm{kg} / \mathrm{m}^{3}$ | Specific <br> volume of <br> vapor $\mathrm{m}^{3} / \mathrm{kg}$ | Enthalpy <br> $(\mathrm{kJ} / \mathrm{kg})$ |  | Entropy <br> $(\mathrm{kJ} / \mathrm{kg}-\mathrm{K})$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | P | $\mathrm{\rho}^{\mathrm{I}}$ | $\mathrm{V}^{\mathrm{v}}$ | $\mathrm{H}^{\mathrm{L}}$ | $\mathrm{H}^{\mathrm{v}}$ | $\mathrm{S}^{\mathrm{L}}$ | $\mathrm{S}^{\mathrm{v}}$ |
| 261.15 | 0.18516 | 1331.8 | 0.10749 | 184.16 | 391.55 | 0.9410 | 1.7351 |
| 309.15 | 0.91172 | 1163.2 | 0.02241 | 250.41 | 417.78 | 1.1715 | 1.7129 |
| 313.15 | 1.0165 | 1146.5 | 0.01999 | 256.35 | 419.58 | 1.1903 | 1.7115 |

Figure 1. DePriester Chart at high temperature

