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| UNIVERSITY OF PETROLEUM AND ENERGY STUDIES  <br> End Semester Examination, Jan- 2021  <br> Course: FLUID FLOW AND HEAT TRANSFER EQUIPMENT DESIGN  <br> Semester: I  <br> Program: M. TECH. CHEMICAL ENGINEERING (PDE)  <br> Course Code: CHPD7005  <br> Instructions: Attempt All Questions  |  |  |  |
| SECTION A |  |  |  |
| S. No. | ATTEMPT ALL QUESTIONS- (5*6=30 MARKS) | Marks | CO |
| Q. 1 | Illustrate the term best efficiency point in Centrifugal pumps. | 5 | CO1 |
| Q. 2 | Explain the term compressor ratio. What is the recommended values for compressor ratio for reciprocating and centrifugal compressors? | 5 | CO4 |
| Q. 3 | Discuss the term 'Class Location 'in fluid carrying pipeline system | 5 | CO1 |
| Q. 4 | Describe 'Affinity Law' for centrifugal pumps. | 5 | CO3 |
| Q. 5 | Illustrate the difference between Recuperative and Regenerative type of Heat Exchangers. | 5 | CO4 |
| Q. 6 | Review ‘TEMA Analysis’ for Heat Exchangers design. With an example, demonstrate the significance of the three letters in a typical TEMA code. | 5 | CO5 |
| SECTION BATTEMPT ALL QUESTIONS $(10 * 5=50)$ |  |  |  |
| Q. 7 | Derive the heat transfer, conduction equation in Cartesian coordinates. | 10 | CO4 |
| Q. 8 | Explain performance curves for centrifugal pumps, | 10 | CO5 |
| Q. 9 | Analyze and explain the algorithm used for Design of Shell and tube heat exchanger (Only steps required) | 10 | CO5 |
| Q. 10 | Explain five significant points on -‘selection criterion' for choosing a specific type of Heat Exchanger. | 10 | CO3 |
| Q. 11 | Reproduce at least twenty main components of Heat Exchanger (only component names are required) | 10 | CO2 |

## SECTION-C <br> (ATTEMPT ANY ONE QUESTION) <br> MISSING DATA ARE TO BE SUITABLY ASSUMED

Q. 12 The Salaya - Mathura oil pipeline is used for transporting oil from Salaya to Mathura refinery. There are two intermediate stations, one at Viramgram and the other one at Koyli. The length of Salaya- Mathura pipeline is 48 miles and is of 18 inch in diameter, with 0.281 inch wall thickness. It is constructed of 5LX-65 grade steel. At origin station Salaya, crude oil of specific gravity 0.85 and 10 cSt viscosity enters the pipeline at a flow rate of $6000 \mathrm{bbl} . / \mathrm{hr}$. At first intermediate station Viramgram (milepost 22) a new stream of crude oil with a specific gravity of 0.82 and 3.5 cSt viscosity enters the pipeline at a flow rate of $1000 \mathrm{bbl} . / \mathrm{hour}$. The mixed stream then continues to another intermediate station Koyli (milepost 32) where 3000 bbl. / hour is stripped off the pipeline. The remaining volume continues to the end of the pipeline at delivery station Mathura.
(a) Evaluate the pressure required at origin station Salaya and the composition of the crude oil arriving at terminus Mathura at a minimum delivery pressure of 50 psi . Assume elevations at Salaya, Viramgram, Koyli, and Mathura to be 100, 150, 250, and 300 feet, respectively. Use the Modified Colebrook-White equation for pressure drop calculations and assume a pipe roughness of 0.002 inches.
(b) Evaluate, the pump HP that will be required at Salaya to maintain this flow rate, assuming 50 -psi pump suction pressure at Salaya and $80 \%$ pump efficiency?
(c) If a positive displacement (PD) pump is used to inject the stream at Viramgram, solve for pressure and HP are required at Viramgram?

## APPENDIX TABLE 1:

## 1. Frictional Pressure drop equation in oil pipelines

$$
\mathrm{Pm}=0.0605 \mathrm{fQ}^{2}\left(\mathrm{Sg} / \mathrm{D}^{5}\right)
$$

## Reynolds No. for Crude Oil Pipelines

a) $\mathrm{R}=92.24 \mathrm{Q} /(\mathrm{v} \mathrm{D})$

Where: $\mathrm{Q}=$ Flow rate, $\mathrm{bbl} /$ day; $\mathrm{D}=$ Internal diameter, in.; v = Kinematic viscosity, cSt
b) $\mathbf{R}=\mathbf{3 5 3 , 6 7 8} \mathbf{Q} /(v D)$

Where: $\mathrm{Q}=$ Flow rate, $\mathrm{m}^{3} / \mathrm{hr}$.; $\mathrm{D}=$ Internal diameter, $\mathrm{mm} ; \mathrm{v}=$ Kinematic viscosity, cSt; $\mathrm{D}=$ Pipe internal diameter, in.

## 2. Modified Colebrook White Equation

$$
\frac{1}{\sqrt{f}}=-2 \log _{10}\left(\frac{e}{3.7 D}+\frac{2.825}{\operatorname{Re} \sqrt{f}}\right)
$$

## 3. Coversion Equations for SSU to Centistokes

$$
\begin{array}{lc}
\text { Centistokes }=0.226(S S U)-\frac{195}{S S U} & 32 \leq S S U \leq 100 \\
\text { Centistokes }=0.220(S S U)-\frac{135}{S S U} & S S U \succ 100
\end{array}
$$

4. BHP required to pump the liquid

$$
B H P=\frac{Q P}{2449 E}
$$

$$
\mathbf{Q}=\text { flow rate }(\text { barrel per hr. }) \quad \mathbf{P}=\text { Differentia pressure }(\mathrm{psi})
$$

## 5. Head to pressure conversion:

Head $=\frac{2.31 \mathrm{psig}}{G}(U S C S)$
6. Specific gravity of blended liquids

$$
S_{b}=\frac{Q_{1} S_{1}+Q_{2} S_{2}+\ldots \ldots Q_{n} S_{n}}{Q_{1}+Q_{2}+\ldots . Q_{n}}
$$



Pipe CD is NPS 10, 0.250 in. wall thickness; and DE is NPS 12, 0.250 in. wall thickness. The delivery pressure at E is fixed at 600 psig. The pipe lengths are as follow: $\mathrm{AB}=12$ miles; $\mathrm{BC}=18$ miles; $\mathrm{CD}=20$ miles; $\mathrm{DE}=8$ miles

The gas gravity is 0.60 , and the flow temperature is $60^{\circ} \mathrm{F}$. The compressibility factor and transmission factor can be assumed to be 0.85 and 20 , respectively, throughout the pipeline. The base pressure and base temperature are 14.7 psia and $60^{\circ} \mathrm{F}$, respectively. Also, calculate the loop length if a particular length of AB is looped with a diameter of 10 NPS and 0.25 -inch wall thickness.

NPS12 $=12.75$ inches; NPS $10=10.75$ inches.

## APPENDIX TABLE 2:

## 1. Equivalent diameter equation

$$
D_{e}=D_{1}\left[\left(\frac{1+\text { Const }}{\text { Const }}\right)^{2}\right]^{1 / 5} \quad \text { Const }=\sqrt{\left(\frac{D_{1}}{D_{2}}\right)^{5}\left(\frac{L_{2}}{L_{1}}\right)}
$$

## 2. Pressure drop equation for gas pipelines

$Q=77.54\left(\frac{T_{b}}{P_{b}}\right)\left(\frac{P_{1}^{2}-P_{2}^{2}}{G T_{f} L Z f}\right)^{0.5} D^{2.5}$
3. Reynolds Equation for Gas Pipelines
$\mathrm{Re}=0.5134\left(\frac{P_{b}}{T_{b}}\right)\left(\frac{G Q}{\mu D}\right)$
$\operatorname{Re}=0.0004778\left(\frac{P_{b}}{T_{b}}\right)\left(\frac{G Q}{\mu D}\right)$

