## Name:

Enrolment No:

## U UPES

## UNIVERSITY OF PETROLEUM AND ENERGY STUDIES End Semester Examination, Dec 2020

Programme Name: B.Tech. (APEG)<br>Course Name : Production Engineering<br>Course Code : PEAU3008<br>Semester : V<br>Nos. of page(s) : 5

## Instructions:

1. All questions are compulsory.
2. Assume any missing data, if any

| S. No. | Section - A (6x5 = 30) <br> (Multiple Choice Question) | Marks | CO |
| :---: | :---: | :---: | :---: |
| Q1 | Determine the apparent molecular weight of the natural gas. The composition of the natural gas in mole fraction: $\mathrm{C} 1=0.805, \mathrm{C} 2=0.093$, $\begin{aligned} & \mathrm{C} 3=0.011, \mathrm{i}-\mathrm{C} 4=0.006, \mathrm{n}-\mathrm{C} 4=0.002, \mathrm{i}-\mathrm{C} 5=0.003, \mathrm{n}-\mathrm{C} 5=0.008, \mathrm{C} 6= \\ & 0.001, \mathrm{C} 7=0.001, \mathrm{~N} 2=0.070 . \end{aligned}$ <br> a) 17.560 <br> b) 19.556 <br> c) 20.612 <br> d) 22.843 | 5 | CO1 |
| Q2 | Determine pseudo-critical pressure of the natural gas in psia. The composition of the natural gas in mole fraction: $\mathrm{C} 1=0.805, \mathrm{C} 2=0.093$, $\mathrm{C} 3=0.011, \mathrm{i}-\mathrm{C} 4=0.006, \mathrm{n}-\mathrm{C} 4=0.002, \mathrm{i}-\mathrm{C} 5=0.003, \mathrm{n}-\mathrm{C} 5=0.008, \mathrm{C} 6=$ $0.001, \mathrm{C} 7+=0.001, \mathrm{~N} 2=0.070$. <br> a) 440 <br> b) 520 <br> c) 670 <br> d) 780 | 5 | CO1 |
| Q3 | The density of the natural gas having specific gravity 0.7 at 2000 psia and $200^{\circ} \mathrm{F}$ (Assume $\mathrm{z}=0.9$ ) in $\mathrm{lbm} / \mathrm{ft} 3$ is <br> a) 4.31 <br> b) 5.02 <br> c) 5.48 <br> d) 6.37 | 5 | CO1 |
| Q4 | When the particle size is reduced by half then terminal settling velocity <br> a) increase by 2 times <br> b) decreases by 2 times | 5 | CO 2 |


|  | c) increases by 4 times <br> d) decreases by 4 times |  |  |
| :---: | :---: | :---: | :---: |
| Q5 | For the reaction between $18 \mathrm{wt} \% \mathrm{HCl}$ solution and calcite, Calculate the gravimetric dissolving power of the acid solution. <br> a) 0.20 <br> b) 0.25 <br> c) 0.30 <br> d) 0.35 | 5 | $\mathrm{CO5}$ |
| Q6 | A sandstone formation has a poison's ratio of 0.20 . If the effective vertical stress acting on the formation is 9000 psi. Calculate the effective horizontal stress in psi <br> a) 1050 <br> b) 2250 <br> c) 2300 <br> d) 9000 | 5 | CO6 |
|  | Section - B (5x10 = 50) |  |  |
| Q1 | Find a conical roof carbon steel tank to store 20,000 barrels of crude oil, using the API 650 standard, it is established that the outlet diameter of the liquid nozzle (Low Type) is 14 " | 10 | $\mathrm{CO3}$ |
| Q2 | Calculate absolute open flow potential and productivity index of a vertical well in an oil reservoir at steady-state radial flow conditions. The following data are given: <br> Porosity $=0.25$ <br> Effective Horizontal Permeability $=10 \mathrm{md}$ <br> Pay Zone Thickness $=50$ feet <br> Average reservoir pressure $=5000 \mathrm{psia}$ <br> Fluid Formation volume factor $=1.2$ <br> Fluid Viscosity $=1.5 \mathrm{cP}$ <br> Drainage Area $=640$ acres <br> Wellbore radius $=0.328$ feet <br> Skin Factor $=5$ | 10 | $\mathrm{CO4}$ |
| Q3 | A $20 \mathrm{wt} \% \mathrm{HCl}$ is needed to propagate wormholes 2 feet from a 0.328 feet radius wellbore in a limestone formation (Specific gravity 2.71) with a porosity of 0.12 . The designated injection rate is $0.12 \mathrm{bbl} / \mathrm{min}-\mathrm{ft}$, the diffusion coefficient is $10^{-9} \mathrm{~m}^{2} / \mathrm{sec}$, and the density of the $20 \% \mathrm{HCL}$ is 1.11 | 10 | $\mathrm{CO5}$ |


|  | $\mathrm{g} / \mathrm{cm}^{3}$. In linear core floods, 1.2 pore volume is needed for wormhole breakthrough at the end of the core. Calculate the following : <br> a) Acid capillary number <br> b) Acid volume requirement in gal/ft., using volumetric model |  |  |
| :---: | :---: | :---: | :---: |
| Q4 | A gas reservoir has a permeability of 5 md . A vertical well of 0.328 feet radius draws the reservoir from center of an area of 320 acres. If the well is hydraulically fractured to create a 2000 feet long, 0.15 inches wide fracture of 200000 md permeability around the center of the drainage area. What would be the fold of increase in well productivity? | 10 | CO6 |
| Q5 | Calculate the maximum width and stress intensity of a fracture with halflength is 12 m and pressurized to 21 MPa , immersed within an elastic medium with $\mathrm{E}=1.2 \mathrm{GPa}$ and poison's ratio $=0.20$, and subjected to far field stress of 20 MPa | 10 | CO6 |
|  | Section-C (1x20 = 20) |  |  |
| Q1 | a) Draw the schematic diagram of vertical heater treater mentioning all the sections with labelling. <br> b) Find the effective length of the coalescing section of horizontal heater treater for the following condition: <br> Oil flow rate: 5000 BOPD <br> Specific gravity of oil $=30^{\circ}$ API <br> Viscosity of oil $=16 \mathrm{cP}$ <br> Diameter of the heater treater $=96$ inches <br> Inlet oil temperature $=80^{\circ} \mathrm{F}$ <br> Short-Circuit Factor $(\mathrm{F})=0.9$ <br> Water $\mathrm{SG}=1.04$ <br> Inlet BS\&W $=10 \%$ <br> Outlet BS\&W $=1 \%$ | 2x10 | CO2 |

Table 1: Typical Sizes and Correspsonding Nominal Capacities for Tanks (API 650)

|  |  | Capacity <br> Tank <br> Diameter, <br> ft. <br> ft. of | Tank Height (ft.) / Number of Courses in Completed Tank        <br> barrels        | $\mathbf{1 6 / 2}$ | $\mathbf{2 4 / 3}$ | $\mathbf{3 2 / 4}$ | $\mathbf{4 0 / 5}$ | $\mathbf{4 8 / 6}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1 0}$ | 14 | 225 | 335 | 450 | - | - | - | - |
| $\mathbf{1 5}$ | 31.5 | 505 | 755 | 1010 | 1260 | - | - | - |
| $\mathbf{2 0}$ | 56 | 900 | 1340 | 1790 | 2240 | 2690 | - | - |
| $\mathbf{2 5}$ | 87.4 | 1400 | 2100 | 2800 | 3500 | 4200 | 4900 | 5600 |
| $\mathbf{3 0}$ | 126 | 2020 | 3020 | 4030 | 5040 | 6040 | 7050 | 8060 |
| $\mathbf{3 5}$ | 171 | 2740 | 4110 | 5480 | 6850 | 8230 | 9600 | 10980 |
| $\mathbf{4 0}$ | 224 | 3580 | 5370 | 7160 | 8950 | 10740 | 12540 | 14340 |
| $\mathbf{4 5}$ | 283 | 4530 | 6800 | 9060 | 11340 | 13600 | 15880 | 18140 |
| $\mathbf{5 0}$ | 350 | 5600 | 8400 | 11200 | 14000 | 16800 | 19600 | 22400 |
| $\mathbf{6 0}$ | 504 | 8060 | 12100 | 16130 | 20160 | 24190 | 28220 | 26130 |
| $\mathbf{7 0}$ | 685 | 10960 | 16450 | 21950 | 27440 | 32930 | - | - |
| $\mathbf{8 0}$ | 895 | 14320 | 21500 | 28670 | 35840 | 35810 | - | - |
| $\mathbf{9 0}$ | 1133 | 18130 | 27220 | 36290 | 45360 | - | - | - |
| $\mathbf{1 0 0}$ | 1399 | 22380 | 33600 | 44800 | - | - | - | - |
| $\mathbf{1 2 0}$ | 2014 | 32250 | 48380 | 54200 | - | - | - | - |
| $\mathbf{1 4 0}$ | 2742 | 43900 | 64860 | - | - | - | - | - |
| $\mathbf{1 6 0}$ | 3581 | 57340 | 74600 | - | - | - | - | - |
| $\mathbf{1 8 0}$ | 4532 | 72570 | - | - | - | - | - | - |
| $\mathbf{2 0 0}$ | 5595 | 89600 | - | - | - | - | - | - |
| $\mathbf{2 2 0}$ | 6770 | 108410 | - | - | - | - | - | - |

Table 2 : Dimensions for Shell Nozzles in Inches. (API 650)

|  | Outside <br> NPS <br> (Size of <br> Nozzle) | of Pipe, <br> OD | Minimum Distance From <br> Bottom of Tank to Center of <br> Nozzle |
| :---: | :---: | :---: | :---: |
| 60 |  |  |  |
| 54 | 54 | 64.625 | 60.375 |
| 52 | 52 | 58.625 | 54.375 |
| 50 | 50 | 56.625 | 52.375 |
| 48 | 48 | 54.625 | 50.375 |
| 46 | 46 | 50.625 | 48.375 |
| 44 | 44 | 48.625 | 46.375 |
| 42 | 42 | 46.625 | 44.375 |
| 40 | 40 | 44.625 | 42.375 |
| 38 | 38 | 42.625 | 40.375 |
| 36 | 36 | 40.625 | 36.375 |
| 34 | 34 | 38.625 | 34.375 |
| 32 | 32 | 36.625 | 32.375 |
| 28 | 28 | 34.625 | 30.375 |
| 26 | 26 | 32.625 | 28.375 |
| 24 | 24 | 30.625 | 26.375 |
| 22 | 22 | 29 | 24.375 |
| 20 | 20 | 27 | 22.375 |
| 18 | 18 | 25 | 20.375 |
| 16 | 16 | 23 | 18.375 |
| 14 | 14 | 21 | 16.375 |
| 12 | 12.75 | 19 | 14.375 |
| 10 | 10.75 | 17.75 | 13.2 |
| 8 | 8.625 | 15.75 | 11.2 |
| 6 | 6.625 | 13.75 | 9.2 |
| 4 | 4.5 | 12.125 | 7.875 |
| 3 | 3.5 | 10.25 | 6 |
| 2 | 2.375 | 9.5 | 5.25 |
|  |  |  |  |

