

UNIVERSITY OF PETROLEUM AND ENERGY STUDIES

End Semester Examination, Dec 2019

Program Name : B.Tech GIE & B.Tech GSE Semester : V

Nos. of page(s) : Five only

Instructions: *Answer should be precise & to the point.*

SECTION A

| S. No. | | | Marks | CO |
|--------|--|--|-------------------|-----|
| Q 1 | i. | You are the company man on a well being drilled. Well takes a kick. What | | CO4 |
| | | will be your course of action? Name the steps you will take to kill the well. | | CO1 |
| | ii. | Explain the procedure to decide casing setting depth. | 4 marks | COI |
| | iii. | "Wells are designed telescopically", discuss your views to justify it. | each (4x5=20) | CO1 |
| | iv. | Compare rotary steering system with mud motor system. | (20) | CO1 |
| | v. | If a well encounters problems during drilling and due to this problem the | | |
| | | approved budget fails, which two decisions should be made? | | CO4 |
| | | SECTION B | | |
| Q 2 | has a depth was the A 8 I formation overbuse the | Il was drilled to a depth of 11,500 ft using 11.0 ppg drilling mud. The drillstring float valve at the bottom of the string. When new drilling mud was pumped to a of 6,500 ft, collapse pressure at the bottom was calculated to be 500 psi. What he density of the new mud? OR 1/2" diameter hole is drilled up to 7,500 ft with a density of 12.5 ppg. If the ation pore pressure at this point is 4500 psi. Calculate i) mud pressure alance above the pore pressure, ii) if the mud density is 10.5 ppg, what would be overbalance, and iii) if the fluid level in the annulus is dropped to 250 ft due to quate hole fill up during tripping, what would be the effect on bottom-hole are? | 8 2+2+4=8 | CO2 |

| Q 3 | List out the various major deflection tools currently used in oil & gas industry for Directional Drilling. Explain in details about any one of them? | 3+5=8 | CO4 |
|-----|--|-------------------|-----|
| Q 4 | What is the objective of well completion? Discuss advantages and disadvantages of both Open Hole and Cased Hole completion. | 3+=8 | CO1 |
| Q 5 | A drilling engineer wants to prepare a drilling mud of volume of 5,550 cubic feet using water and Bentonite of 2.43 gm/cc density. The required final weight was calculated to be 9.5 ppg. Calculate the amount of Bentonite to be mixed in tons and the volume of water to be used in barrels. OR Draw a neat flow diagram of Mud Circulation System. Briefly explain the function of any five component available on this system. | 4+4=8 3+5=8 | CO2 |
| Q 6 | A bladder type accumulator bottle of 11 gallons capacity was pre-charged with Nitrogen gas at pressure of 1000Psi. The hydraulic fluid is pumped to its rated pressure of 3000 Psi. This Hydraulic fluid of bottle was used to operate BOP function. The pressure of the bottle has dropped to 1250 psi. The volume of bladder and puppet assembly in the accumulator bottle is one gallon. Calculate how much fluid has been used to operate the BOP functions? | 8 | CO2 |
| | SECTION-C | | |
| Q 7 | The hoisting system of a rig derrick has a load of 350,000 lbf. The input power of the drawworks for the rig can be a maximum of 530 hp. Eight drilling lines are strung between the crown block and traveling block. Assume that the rig floor is arranged as shown in Figure 2.3. Consider there is some loss of power due to friction within the hoisting system. Compute (1) the static tension in the fast line when upward motion is impending, (2) the mechanical advantage of the block and tackle, (3) the maximum hook horsepower available, (4) the maximum hoisting speed, (5) if a 90 ft stand is required to be pulled, what should be the required time, (6) the actual derrick load, (7) the maximum equivalent derrick load, and (8) the derrick efficiency factor. | 2.5x8=20 | CO2 |
| | OR | | |
| | (a) A production casing was planned to be set in the well with drilling mud of 9.8 ppg at the annulus. When inside casing was filled with cement slurry of 15.8 ppg mud, burst safety factor was calculated to be 2.50. When cement slurry displaced and filled the annulus, mud weight of the drilling fluid inside the casing was 9.8 ppg. Collapse safety factor was calculated to be 2.27 when cement slurry was totally filled the annulus. Determine the ratio between burst and collapse ratings of the casing. In addition, if the burst rating of the casing is 11,300 psi, calculate collapse resistance of the casing and the casing setting depth. | 4+4+4=12 4+4=8 | |

| Q8 | (b) What do you understand by the term "The Author (AFE)". Also discuss the key factors which affect the Original mud weight | - | | |
|----|--|--|---------|-----|
| | Measured depth | = 10,525 ft | | |
| | Kill rate pressure @ 50 spm | = 1000 psi | | |
| | Drill string: | = 0.01776 bbl/ft | | |
| | drill pipe 5.0 in. — 19.5 lb/ft capacity HWDP 5.0 in. 49.3 lb/ft | - U.U1 / / O DDI/1t | | |
| | capacity | = 0.00883 bbl/ft | | |
| | length | = 250 ft | | |
| | drill collars 8.0 in. OD — 3.0 in. ID | 0.00071.11/6 | | |
| | capacity length | = 0.0087 bbl/ft = 350 ft | | |
| | Annulus: | - 550 It | | |
| | hole size | = 12 1/4 in. | | |
| | drill collar/open hole capacity | = 0.0836 bbl/ft | | |
| | drill pipe/open hole capacity | = 0.1215 bbl/ft | | |
| | drill pipe/casing capacity Mud pump (7 in, y 12 in, tripley @ 95% eff.) | = 0.1303 bbl/ft = 0.136 bbl/stk | | |
| | Mud pump (7 in. x 12 in. triplex @ 95% eff.) Leak-off test with 9,0 ppg mud | = 0.130 bbl/stk = 1130 psi | | |
| | Casing setting depth | = 4000 ft | | |
| | Shut-in drill pipe pressure | = 450 psi | | CO3 |
| | Shut-in casing pressure | = 550 psi | 2x10=20 | |
| | Pit volume gain True vertical depth | = 40 bbl = 10,000 ft | | |
| | True vertical deptil | - 10,000 It | | |
| | Use the above data to answer the following questions. | | | |
| | (A) SURFACE TO BIT STROKES | | | |
| | (B) BIT TO SHOE STROKES | 00 100 100 100 100 100 100 100 100 100 | | |
| | (C) BIT TO SURFACE VOLUME | | | |
| | (D) KILL MUD WEIGHT | | | |
| | (E) INITIAL CIRCULATING PRESSURE | | | |
| | (F) FINAL CIRCULATING PRESSURE | AND ADD TO THE RESIDENCE OF THE PARTY OF THE | | |
| | (G) MAASP WITH CURRENT MUD WEIGHT | | | |
| | (H) MAASP AFTER CIRCULATING KILL MUD | | | |
| | (I) TIME FOR COMPLETE ONE CIRCULATION | And | | |
| | (J) PRESSURE DROP PER 100 STROKES | and the solution and the first the solution and the solut | | |
| | | | | |

Please detach the Kill Sheet from the question paper, fill it up & tie it with the answer sheet.

Formation Strength Data: Current Well Data: Surface Leak-off Pressure (A) psi Mud data: Mud Weight (B) ppg Maximum Allowable Mud Weight Mud Weight ppg (B) +Shoe True Vertical Depth x 0.052 Casing Shoe Data: ppg Initial MAASP Size in. {(C) -Current Mud Weight} x Shoe TVD x 0.052 ft. M.D. psi ft. T.V.D. Pump No.1 Pump No.2 Displacement Displacement Hole Data: bbls /stroke bbls / stroke Slow Dynamic Pressure, Loss (PL) Size in. Pump Pump No. 1 Pump No. 2 Rate Data M.D. ft. Spm T.V.D. ft. Spm Pre-Volume Data: Length Capacity Volume **Pump Strokes** Time Bbls/ft. Bbls minutes Drill Pipe Volume Pump Strokes Heavy Wall Drill Pipe = Pump Displacement Slow Pump Drill Collars X = Rate **Drill String Volume** (E) stks (D) bbl DC x Open Hole X DP/HWDP x Open Hole × **Open Hole Volume** (F) bbl stks min = (G) bbl DP x Casing X stks min **Total Annulus Volume** (F+G) = (H)stks min **Total Well System Volume** (D+H) = (1)bbl stks min

API Field Unit

Surface BOP (Vertical Well) Kill Sheet

| psi SIC | psi SICP | psi | Pit Gain | bbls | |
|---------------|--------------------------|---|-----------|-------------------|--|
| Current Mud V | Current Mud Weight + | SIDPP TVD X 0.052 | | | |
| | | | | | |
| Dynamic Pres | Dynamic Pressure Los | s + SIDPP | | /// | |
| | | | - | = psi | |
| | Current Mud Weight | x Dynamic Pressure Loss urrent Mud Weight | | | |
| | = ps | (E) | | psi / 100 strokes | |
| ure S | Static & I Drill Pipe | Static & Dynamic Drill Pipe Pr.(psi) | | | |
| F r e e s | P r e s u r e | | | | |
| | | s s u r e | S S U r e | s s u r | |

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