| Name: <br> Enrolment No: |  |  |  |
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| UNIVERSITY OF PETROLEUM AND ENERGY STUDIESEnd Semester Examination, December 2019Course: Engineering ThermodynamicsProgram: B. Tech. (APE-Gas)Course Code: MECH 2001Instructions: Assume any missing data. The notations used here have the usual meanings. Draw the diagrams,wherever necessary. |  |  |  |
| SECTION - A ( $\mathbf{2} \times \mathbf{1 0}=\mathbf{2 0}$ marks) <br> (Answer all the questions) |  |  |  |
| S. <br> No. |  | Marks | CO |
| 1. | A stream of warm water is produced in a steady flow mixing process by combining 1 $\mathrm{kg} / \mathrm{s}$ of cold water at 298.15 K with $0.8 \mathrm{~kg} / \mathrm{s}$ of hot water at 348.15 K . During mixing, heat is lost to surroundings at the rate of 30 kW . What is the temperature of the warm water stream? Assume the specific heat of water is $4.18 \mathrm{~kJ} / \mathrm{kg}-\mathrm{K}$. | 10 | CO2 |
| 2. | Explain absorption refrigeration system with the help of a schematic diagram. Derive a relation to estimate the COP of absorption refrigeration system. | 10 | CO5 |
| SECTION - B ( $5 \times 12=60$ marks $)$ <br> (Answer all the questions) |  |  |  |
| 3. | An inventor has devised a complicated nonflow process in which 1 mol of air is the working fluid. The net effects of the process are claimed to be: <br> - A change in state of air from 523.15 K and 3 bar to 353.15 K and 1 bar <br> - A production of 1800 J of work <br> - The transfer of an undisclosed amount of heat to a heat reservoir at 303.15 K Determine whether the claimed performance of the process is consistent with the second law. Assume that air is an ideal gas for which $C_{p}=(7 / 2) R$. | 12 | CO2 |
| 4. | A mass $m$ of liquid water at temperature $T_{1}$ is mixed adiabatically and isobarically with an equal mass of liquid water at temperature $\mathrm{T}_{2}$. Assuming constant $\mathrm{C}_{\mathrm{p}}$, show that $S_{G}=2 m C_{p} \ln \frac{\left(T_{1}+T_{2}\right) / 2}{\sqrt{T_{1} T_{2}}}$ | 12 | CO2 |


|  | and prove that this is positive. What would be the result if the masses of water were different, say $\mathrm{m}_{1}$ and $\mathrm{m}_{2}$. |  |  |  |  |  |  |  |  |
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| 5. | Calculate Z and V for ethane at 323.15 K and 15 bar by the following equations: <br> (a) the truncated virial equation, with the following experimental values of virial coefficients: $\mathrm{B}=-156.7 \mathrm{~cm}^{3} / \mathrm{mol}, \mathrm{C}=9650 \mathrm{~cm}^{6} / \mathrm{mol}^{2}$. <br> (b) the truncated virial equation, with the value of B from generalized Pitzer correlations. Virial coefficients $B^{0}$ and $B^{1}$ are: $B^{0}=0.083-\frac{0.422}{T_{r}^{1.6}} \text { and } B^{1}=0.139-\frac{0.172}{T_{r}^{4.2}}$ <br> For ethane: $\mathrm{T}_{\mathrm{c}}=305.3 \mathrm{~K}, \mathrm{P}_{\mathrm{c}}=48.72$ bar and $\omega=0.1$. |  |  |  |  |  |  | 12 | CO 3 |
| 6. | 1 kmol of ethylene is contained in a $0.6 \mathrm{~m}^{3}$ steel vessel immersed in a constant temperature bath at $200{ }^{\circ} \mathrm{C}$. Determine the pressure developed by the gas by each of the following: <br> (a) ideal gas equation <br> (b) van der Waals equation <br> (c) Redlich/Kwong equation <br> For ethylene: $\mathrm{T}_{\mathrm{c}}=283.1 \mathrm{~K}, \mathrm{P}_{\mathrm{c}}=51.17$ bar and parameters assigned for equations of state are: |  |  |  |  |  |  | 12 | $\mathrm{CO3}$ |
| 7. | A Carnot refrigerator has tetrafluoroethane as the working fluid. For $\mathrm{T}_{\mathrm{C}}=261.15 \mathrm{~K}$ and $\mathrm{T}_{\mathrm{H}}=311.15 \mathrm{~K}$, determine <br> (a) the heat addition per kg of fluid <br> (b) the heat rejection per kg of fluid <br> (c) the mechanical power per kg of fluid for each of the four steps <br> (d) the coefficient of performance $\omega$ for the cycle <br> Thermodynamic properties of Saturated tetrafluoroethane are given in Table 1. |  |  |  |  |  |  | 12 | CO5 |
| SECTION - C ( $\mathbf{1} \times \mathbf{2 0}=\mathbf{2 0}$ marks $)$ <br> (Answer all the questions) |  |  |  |  |  |  |  |  |  |


| 8.(a) <br> (b) | What do you understand by retrograde condensation? Explain with the help of a PT diagram. <br> The expressions for activity coefficient of species 1 and 2 in a binary liquid mixture at a given T and P are: $\begin{aligned} & \ln \gamma_{1}=x_{2}^{2}\left(0.273+0.096 x_{1}\right) \\ & \ln \gamma_{2}=x_{1}^{2}\left(0.273-0.096 x_{1}\right) \end{aligned}$ <br> (i) Determine the implied expression for $\mathrm{G}^{\mathrm{E}} / \mathrm{RT}$. <br> (ii) Generate expressions of $\ln \gamma_{1}$ and $\ln \gamma_{2}$ from the results of (i). | 5 15 | $\mathrm{CO4}$ |
| :---: | :---: | :---: | :---: |
|  | OR |  |  |
| 8.(a) <br> (b) | Develop a general equation for calculation of $\ln \widehat{\emptyset}_{i}$ values from compressibility factor data. <br> Determine the Dew point of a mixture containing $48 \%$ ethane (1), $25 \%$ propane (2), $15 \%$ iso-butane (3) and rest iso-pentane (4) at 333.15 K. K-values for Systems of light hydrocarbons are given in Figure 1. | 8 12 |  |

Table: 1 Thermodynamic properties of Saturated Tetrafluoroethane

| Temperature <br> $(\mathrm{K})$ | Saturation <br> pressure <br> MPa | Liquid <br> density <br> $\mathrm{kg} / \mathrm{m}^{3}$ | Specific <br> volume of <br> vapor $\mathrm{m}^{3} / \mathrm{kg}$ | Enthalpy <br> $(\mathrm{kJ} / \mathrm{kg})$ |  | Entropy <br> $(\mathrm{kJ} / \mathrm{kg}-\mathrm{K})$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | P | $\rho^{\mathrm{I}}$ | $\mathrm{V}^{\mathrm{v}}$ | $\mathrm{H}^{\mathrm{l}}$ | $\mathrm{H}^{\mathrm{v}}$ | $\mathrm{S}^{\mathrm{I}}$ | $\mathrm{S}^{\mathrm{v}}$ |
| 261.15 | 0.18516 | 1331.8 | 0.10749 | 184.16 | 391.55 | 0.9410 | 1.7351 |
| 309.15 | 0.91172 | 1163.2 | 0.02241 | 250.41 | 417.78 | 1.1715 | 1.7129 |
| 313.15 | 1.0165 | 1146.5 | 0.01999 | 256.35 | 419.58 | 1.1903 | 1.7115 |


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Figure 1. K values for Systems of light hydrocarbons - Low Temperature

