Name:

Enrolment No:



UNIVERSITY OF PETROLEUM AND ENERGY STUDIES

End Semester Examination, December 2019

Course: Engineering Thermodynamics Program: B. Tech. (APE-Gas) **Course Code: MECH 2001**

Semester : III Time : 3 hr Max. Marks: 100

Instructions: Assume any missing data. The notations used here have the usual meanings. Draw the diagrams, wherever necessary.

| | SECTION - A (2 × 10 = 20 marks) (Answer all the questions) | | |
|-----------|---|-------|-----|
| S. No. | | Marks | СО |
| 1. | A stream of warm water is produced in a steady flow mixing process by combining 1 kg/s of cold water at 298.15 K with 0.8 kg/s of hot water at 348.15 K. During mixing, heat is lost to surroundings at the rate of 30 kW. What is the temperature of the warm water stream? Assume the specific heat of water is 4.18 kJ/kg-K. | 10 | CO2 |
| 2. | Explain absorption refrigeration system with the help of a schematic diagram. Derive a relation to estimate the COP of absorption refrigeration system. | 10 | CO5 |
| | SECTION - B (5 × 12 = 60 marks) (Answer all the questions) | | |
| 3. | An inventor has devised a complicated nonflow process in which 1 mol of air is the working fluid. The net effects of the process are claimed to be: - A change in state of air from 523.15 K and 3 bar to 353.15 K and 1 bar - A production of 1800 J of work - The transfer of an undisclosed amount of heat to a heat reservoir at 303.15 K Determine whether the claimed performance of the process is consistent with the second law. Assume that air is an ideal gas for which $C_p = (7/2)R$. | 12 | CO2 |
| 4. | A mass m of liquid water at temperature T ₁ is mixed adiabatically and isobarically with an equal mass of liquid water at temperature T ₂ . Assuming constant C _p , show that $S_G = 2 m C_p \ln \frac{(T_1 + T_2)/2}{\sqrt{T_1 T_2}}$ | 12 | CO2 |

| | and prove that this is pos | itive. Wha | t would | be the 1 | result if the | masses of wa | ater were | | |
|----|--|--|-----------|---------------------|----------------------------|---------------|------------|-----|-----|
| | different, say m1 and m2. | | | | | | | | |
| 5. | Calculate Z and V for etha | late Z and V for ethane at 323.15 K and 15 bar by the following equations: | | | | | | | |
| | (a) the truncated virial equation, with the following experimental values of virial | | | | | | | | |
| | coefficients: $B = -156.7 \text{ cm}^3/\text{mol}$, $C = 9650 \text{ cm}^6/\text{mol}^2$. | | | | | | | | |
| | (b) the truncated virial equation, with the value of B from generalized Pitzer correlations. | | | | | | relations. | 12 | CO3 |
| | Virial coefficients B^0 and B^1 are: | | | | | | | | |
| | $B^0 = 0.083 - \frac{0.422}{T_r^{1.6}}$ and $B^1 = 0.139 - \frac{0.172}{T_r^{4.2}}$ | | | | | | | | |
| | For ethane: $T_c = 305.3 \text{ K}$, $P_c = 48.72 \text{ bar and } \omega = 0.1$. | | | | | | | | |
| 6. | 1 kmol of ethylene is co | ontained in | n a 0.6 | m ³ stee | l vessel im | mersed in a | constant | | |
| | temperature bath at 200 °C | C. Determi | ne the pr | essure d | eveloped by | the gas by ea | ch of the | | |
| | following: | | | | | | | | |
| | (a) ideal gas equation | | | | | | | | |
| | (b) van der Waals equation | | | | | | | | |
| | (c) Redlich/Kwong equation | | | | | | | ~~~ | |
| | For ethylene: $T_c = 283.1$ K, $P_c = 51.17$ bar and parameters assigned for equations of | | | | | | 12 | CO3 | |
| | state are: | | | | | | | | |
| | Equation of state | $\alpha(T_r)$ | Σ | E | Ω | Ψ | Zc | | |
| | Van der Waals (vdW) | 1 | 0 | 0 | 1/8 | 27/64 | 3/8 | | |
| | Redlich/Kwong (RK) | $T_r^{-1/2}$ | 1 | 0 | 0.08664 | 0.42748 | 1/3 | | |
| 7. | A Carnot refrigerator has tetrafluoroethane as the working fluid. For $T_C = 261.15$ K and | | | | | | | | |
| | $T_{\rm H} = 311.15$ K, determine | | | | | | | | |
| | (a) the heat addition per kg of fluid | | | | | | | | |
| | (b) the heat rejection per kg of fluid | | | | | | 12 | CO5 | |
| | (c) the mechanical power per kg of fluid for each of the four steps | | | | | | | | |
| | (d) the coefficient of performance ω for the cycle | | | | | | | | |
| | Thermodynamic properties of Saturated tetrafluoroethane are given in Table 1. | | | | | | | | |
| | | | | • | 20 = 20 marl questions) | (S) | | | |

| 8. (a) | What do you understand by retrograde condensation? Explain with the help of a PT | 5 | | | |
|---------------|--|----|------|--|--|
| | diagram. | | | | |
| (b) | The expressions for activity coefficient of species 1 and 2 in a binary liquid mixture at | | | | |
| | a given T and P are: | 15 | | | |
| | $\ln \gamma_1 = x_2^2 (0.273 + 0.096 x_1)$ | | | | |
| | $\ln \gamma_2 = x_1^2 \ (0.273 - 0.096 \ x_1)$ | | | | |
| | (i) Determine the implied expression for G^E/RT . | | ~~ . | | |
| | (ii) Generate expressions of $\ln \gamma_1$ and $\ln \gamma_2$ from the results of (i). | | CO4 | | |
| | OR | | | | |
| 8. (a) | Develop a general equation for calculation of $\ln \hat{\varphi}_i$ values from compressibility factor | 8 | | | |
| | data. | | | | |
| (b) | Determine the Dew point of a mixture containing 48% ethane (1), 25% propane (2), | 12 | | | |
| | 15% iso-butane (3) and rest iso-pentane (4) at 333.15 K. K-values for Systems of light | | | | |
| | hydrocarbons are given in Figure 1. | | | | |

Table: 1 Thermodynamic properties of Saturated Tetrafluoroethane

| Temperature (K) | Saturation pressure MPa | Liquid density kg/m ³ | Specific volume of vapor m ³ /kg | Enthalpy (kJ/kg) | | | Entropy (kJ/kg-K) | | |
|--------------------|-------------------------------|--|---|---------------------|----------------|----------------|----------------------|--|--|
| | Р | ρ^{l} | $\mathbf{V}^{\mathbf{v}}$ | H^1 | H ^v | \mathbf{S}^1 | S ^v | | |
| 261.15 | 0.18516 | 1331.8 | 0.10749 | 184.16 | 391.55 | 0.9410 | 1.7351 | | |
| 309.15 | 0.91172 | 1163.2 | 0.02241 | 250.41 | 417.78 | 1.1715 | 1.7129 | | |
| 313.15 | 1.0165 | 1146.5 | 0.01999 | 256.35 | 419.58 | 1.1903 | 1.7115 | | |

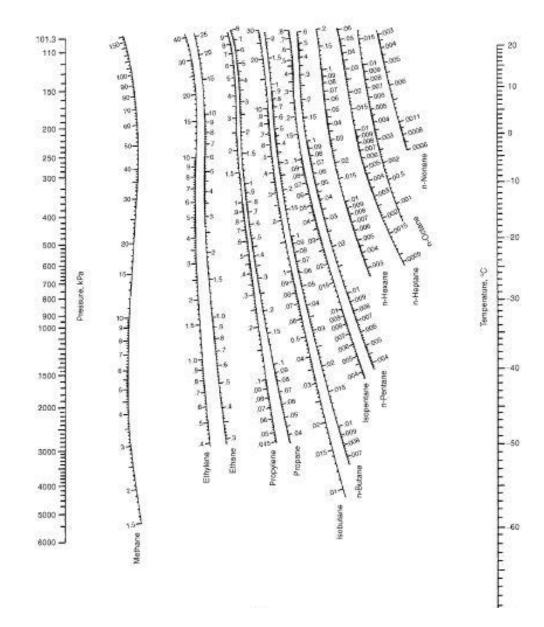


Figure 1. K values for Systems of light hydrocarbons – Low Temperature