| Name: <br> Enrolment No: |  |  |  |
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| Course: $\quad$ Petroleum Transport System \& Operations-1 Semester: 1 <br> Programme: M.Tech. Pipeline Engineering Time: 03 hrs. <br> CODE: CHPL 7004 Max. Marks: $\mathbf{1 0 0}$ <br> Instructions: $\boldsymbol{i}$. Attempt all questions. $\boldsymbol{i i}$. Missing data can be suitably assumed  |  |  |  |
| SECTION A |  |  |  |
| S. No. |  | Marks | CO |
| Q1 | Define compressor ratio for a centrifugal and reciprocating compressors. | 5 | CO1 |
| Q2 | Differentiate between $\mathrm{NPSH}_{\mathrm{A}}$ and $\mathrm{NPSH}_{\mathrm{R}}$ | 5 | CO2 |
| Q3 | Explain Line Pack volume and Line Fill Volume | 5 | CO2 |
| Q4 | Explain the term "Adiabatic efficiency" and hydraulic balance in compressors. | 5 | CO3 |
| SECTION B |  |  |  |
| Q5 | Explain the reasons that lead to Gas Hydrates formation in Pipelines and the preventive measures that can be taken to avoid them in subsea pipelines | 10 | CO5 |
| Q6 | A 16 in. crude oil pipeline ( 0.250 in. wall thickness) having internal roughness of 0.002 inches, is 30 miles long from point A to point B . The flow rate at the inlet A is 4000 bbl . / hr. The crude oil properties are specific gravity of 0.85 and viscosity of 10 cSt at a flowing temperature of $70^{\circ} \mathrm{F}$. (a) Calculate the pressure required at A without any pipe loop. Assume, 50 psi, delivery pressure at the terminus B and a flat pipeline elevation profile. (b) If a 10 mile, portion $C D$, starting at milepost 10 is, looped with an identical 16 in. pipeline, calculate the reduced pressure at A. | 10 | CO1 |
| Q7 | Calculate the compressor horsepower required for an adiabatic compression of 106 MMSCFD gas with inlet temperature of $68^{\circ} \mathrm{F}$ and 725 psia pressures. The discharge pressure is 1305 psia . Assume the compressibility factors at suction and discharge conditions to be $Z_{1}=1.0$ and $Z_{2}=0.85$, respectively, and the adiabatic exponent $=$ 1.4 , with the adiabatic efficiency $=0.8$. If the mechanical efficiency of the compressor driver is 0.95 , what BHP is required? Also, calculate the outlet | 10 | CO1 |


|  | temperature of the gas. |  |  |
| :---: | :---: | :---: | :---: |
| Q8 | Explain the reasons for the two-phase flow in pipelines. Also, explain with figures the different flow patterns observed in two-phase flow. Explain the Bakers Chart to identify the flow pattern in multiphase flow | 10 | CO5 |
| SECTION-C |  |  |  |
| Q9 | In the Figure 1, shown below, the pipeline from station A to station B is 48 miles long and is 18 in . in nominal diameter, with 0.281 in . wall thickness. It is, constructed of 5LX-65 grade steel. At station A, crude oil of specific gravity, 0.85 and 10 cSt viscosity enters the pipeline at a flow rate of 6000 barrel per hour. At station, C (milepost-22) a new stream of crude oil with specific gravity of 0.82 and 3.5 cSt viscosity enters the pipeline at a flow rate of 1000 barrel per hour. The mixed stream then continues to station D (milepost 32) where 3000 barrel per hour is, stripped off the pipeline. The remaining volume continues to the end of the pipeline at point $B$. (a) Calculate the pressure required at dispatch station $A$ to deliver the crude oil at station B at a minimum delivery pressure of 50 psi . Also calculate the specific gravity and viscosity of crude oil delivered at station B. Assume elevations at A,C,D and B to be 100, 150, 250 and 300 feet respectively. Use, Colebrook-White equation for pressure drop calculation and assume pipe roughness of 0.002 in . (b) Calculate the BHP required to- maintain 6000 barrel per hour of flow rate at A , assuming 50 psi , pump suction pressure at A and $80 \%$ pump efficiency? (c) If, a positive displacement (PD) pump is used, to inject the stream at C , that itself receives the liquid at 50 psi , and has $80 \%$ efficiency what pressure and HP is required at C . | 20 | $\begin{aligned} & \mathrm{CO1}, \\ & \text { CO2, } \\ & \text { CO3 } \end{aligned}$ |


|  | Figure 1 |  |  |
| :--- | :--- | :--- | :--- |
| Q10 | A natural gas pipeline runs 140 miles from Dadri to Panipat. The pipeline is of NPS <br> $16,0.250$ in. wall thickness. Through calculations, it was found that the pipeline <br> should not be operated at a pressure above 1200 psig. The gas specific gravity and <br> viscosity were found to be 0.6 and $8 \times 10^{-6} \mathrm{lb}$. per feet per second, respectively. The <br> pipe roughness is assumed $700 \mu$ inch, and the base pressure and base temperature are <br> 14.7 psia. and $60^{\circ} \mathrm{F}$, respectively. The gas flow rate is 175 MMSCFD at $80^{\circ} \mathrm{F}$, and <br> the delivery pressure required at Panipat is 800 psig. <br> a) Calculate the pressure required at Dadri to deliver the gas at Panipat at the desired <br> pressure of 800 psig. <br> b) The pipeline operator arbitrary choses to install the compressor station at the <br> midpoint of the pipeline. Show through calculations if the location of compressor <br> station at mid- point is optimum. If not, calculate the exact location of compressor <br> station. Assume $\boldsymbol{Z}=\mathbf{0 . 8 5}$. | $\mathbf{2 0}$$\mathbf{C O 1 ,}$ <br> $\mathbf{C O 3}$ |  |

## APPENDIX

All Notations have their usual meaning and units

1. Reynolds Equation for Gas Pipelines:

$$
\begin{array}{r}
\operatorname{Re}=0.5134\left(\frac{P_{b}}{T_{b}}\right)\left(\frac{G Q}{\mu D}\right)  \tag{SI}\\
\operatorname{Re}=0.0004778\left(\frac{P_{b}}{T_{b}}\right)\left(\frac{G Q}{\mu D}\right)
\end{array}
$$

(USCS)

## 2. Reynolds No. for Crude Oil Pipelines

a) $\quad \mathrm{R}=92.24 \mathrm{Q} /(\mathrm{v} \mathrm{D})$

Where: $\mathrm{Q}=$ Flow rate, $\mathrm{bbl} /$ day; $\mathrm{D}=$ Internal diameter, in.; $v=$ Kinematic viscosity, cSt
b) $\mathbf{R}=\mathbf{3 5 3 , 6 7 8} \mathbf{Q} /(v D)$

Where: $\mathrm{Q}=$ Flow rate, $\mathrm{m}^{3} / \mathrm{hr}$.; $\mathrm{D}=$ Internal diameter, $\mathrm{mm} ; ~ v=$ Kinematic viscosity, cSt
3. Pressure Drop per unit length for oil pipelines (USCS)

$$
\mathrm{Pm}=0.0605 \mathrm{fQ}^{2}\left(\mathrm{Sg} / \mathrm{D}^{5}\right)
$$

$\mathrm{Pm}=$ pressure drop due to friction ( $\mathrm{psi} / \mathrm{mile}$ ); $\mathrm{Q}=$ Liquid flow rate (bbl. per day); $\mathrm{D}=$ Pipe Internal- diameter, in.
4. Colebrook White Equation

$$
\frac{1}{\sqrt{f}}=-2 \log _{10}\left(\frac{e}{3.7 D}+\frac{2.51}{\operatorname{Re} \sqrt{f}}\right)
$$

5. Coversion Equations for SSU to Centistokes

Centistokes $=0.226(S S U)-\frac{195}{S S U}$
$32 \leq S S U \leq 100$

Centistokes $=0.220(S S U)-\frac{135}{S S U}$
6. Horsepower required to compress gas in compressor $\quad S S U \succ 100$
7.

$$
\begin{gathered}
H P=0.0857\left(\frac{\gamma}{\gamma-1}\right) Q T_{1}\left(\frac{Z_{1}+Z_{2}}{2}\right)\left(\frac{1}{\eta_{a}}\right)\left[\left(\frac{P_{2}}{P_{1}}\right)^{\frac{\gamma-1}{\gamma}}-1\right] \begin{array}{l}
\text { Adiabatic Efficienecy of } \\
\text { Compressor }
\end{array} \\
\eta_{a}=\left(\frac{T_{1}}{T_{2}-T_{1}}\right)\left[\left(\frac{z_{1}}{z_{2}}\right)\left(\frac{P_{2}}{P_{1}}\right)^{\frac{\gamma-1}{\gamma}}-1\right]
\end{gathered}
$$

8. BHP required to pump the liquid

$$
B H P=\frac{Q P}{2449 E}
$$

$\mathbf{Q}=$ flow rate (bbl./hr.);
$\mathbf{P}=$ Differentia pressure (psi)
9. Relation between Head and Pressure drop in liquid pipelines

$$
H(\text { feet })=\frac{2.31 p s i}{G}
$$

