Name:

**Enrolment No:** 



## UPES End Semester Examination, December 2024

## Course: Propulsion-II Program: B. Tech ASE Course Code: ASEG3004

Semester : V Time : 03 hrs. Max. Marks: 100

**Instructions:** Make use of sketches/plots to elaborate your answer. Brief and to-the-point, answers are expected. Assume suitable data if needed. Gas Table allowed, Refer attached formula sheet.

## SECTION A (50x4M=20Marks)

	(SQX4M=20Marks)		
S. No.		Marks	CO
Q 1	List the key components of an turbofan and turboprop engine with neat sketch.	4	CO4
2	Describe the differences in working principles between an ramjet and scramjet engine.	4	CO2
3	Apply the concept of A/A* ratios to analyze supersonic nozzle performance and show the plot between area ratio to Mach number with suitable example.	4	CO3
4	Describe how normal shocks affect total pressure in supersonic inlets and suggest the right method to anchor the shock.	4	CO1
5	Evaluate the impact of thermal choking on the overall efficiency of a thermodynamic cycle.	4	CO2
	SECTION B (4Qx10M= 40 Marks)		
Q 6	<ul> <li>Air is discharged from a reservoir at a pressure of 1.2 MPa and temperature of 450 K through a nozzle to an exit pressure of 0.08 MPa. If the flow rate through the nozzle is 3000 kg/h, and assuming isentropic flow, determine <ul> <li>a) The throat area, pressure, and velocity.</li> <li>b) The exit area and Mach number.</li> </ul> </li> </ul>	10	CO3
7	Air enters a convergent -divergent nozzle with stagnation conditions of 400 kPa and 400 K. the area ratio of the nozzle is 4. After passing through the nozzle , the flow enters a duct where heat is added. At the end of duct there is normal shock wave. The stagnation temperature upstream of a shock wave is 500 K. assuming isentropic flow in the nozzle and Rayleigh flow in the duct. Calculate the heat added and the stagnation pressure loss.	10	CO2
8	A 3.5 m long well insulated duct of diameter 50 mm and average friction coefficient 0.005 is connected to a frictionless bell mouth entrance. Air at 110 kPa and 300 K is drawn through the entrance and flows into the duct. Find the maximum mass flow rate , the flow parameters at exit and the range of back pressure that will produce the flow.	10	CO3

	OR		
	<ul> <li>Differentiate between turbojet, turbofan and turboprop engines based on the following parameters.</li> <li>1. Thrust generation</li> <li>2. Efficiency</li> <li>3. Size of the powerplant</li> <li>4. Application</li> <li>5. Schematic diagram</li> </ul>		
9	An aerial vehicle is equipped with a pulsejet engine at an altitude of 1000 ft having diffuser area The vehicle is cruising at a speed of 850 m/s. consider the naphthalene as an fuel and heating value is equal to 49000 kJ/ kg Compute (a) Mass flow rate per unit area (b) thrust power. (c) TSFC SECTION-C	10	C04
	(2Qx20M=40 Marks)		
Q 10	A supersonic wind tunnel is designed for $M=3.0$ . if the air in the reservoir is at a pressure of 1.4 bar and at a temperature of 27 $^{0}$ C, determine the mass flow rate , area of test section and the pressure , temperature and density of air at the nozzle throat and test section. Nozzle throat area is $0.1 \text{ m}^2$ . <b>OR</b> Design an advanced turbofan engine for passenger aircraft operating at an altitude of 35000 ft at 0.6 Mach number with the following data.		
	Bypass ratio = $0.6$ Overall pressure ratio= 23 Fan pressure ratio = $3.5$ Fuel heating value = $46000 \text{ kJ/kg}$ Turbine inlet temperature = $1800 \text{ K}$ Diffuser pressure recovery factor = $0.89$ Axial compressor efficiency = $0.9$ Axial fan efficiency = $0.98$ Burner pressure recovery factor = $0.96$ Turbine efficiency = $0.93$ Nozzle efficiency = $1$	20	CO4
	Calculate the thrust per unit mass flow rate and the TSFC.		

2. The thrust force
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• full-to-air ratio 
$$(f) = \frac{m_{1}^{2}}{m_{a}}$$
  
• Thomentum = malify Ue Tprenue =  $(fe-fa)Ae$   
T = malify Ue-U or T = malue-U  
 $\therefore$  Thrust = malify Ue-U or T = malue-U  
 $\therefore$  Thrust = malify Ue-U or T = malue-U  
 $\therefore$  Thrust = malify Ue-U + mic(Ue-U) + Aeh (Peh-Pa) + Aec(Iec-Pa) - turbofon L  
propendies of the two states (ue-U) =  $\frac{1}{m_{1}(1+f)Ue-U} + Ae(Peh-Pa) + Ae(Peh-Pa)}$   
•  $\pi p$   
 $(prepulsive ff) = \frac{u}{uT + 0.5mie(Ue-U)} = \frac{u \{malif + 1Ue-U\} + Ae(Peh-Pa)\}}{u \{malif + flue-U\} + Ae(Peh-Pa)\}} + (0.5mia(1+f)(Ue-U))}$   
•  $\pi p = \frac{2uT}{malif + flue-U} \Rightarrow Turbofon L prefon$   
•  $\pi p = \frac{2(T T_{-Tc})}{u(Th - Tc}) + ub + uc}$   
 $(old thrust (Th) = minif(1+flue-U] + Aec(Pec-Pa)}{u(Th - Tc}) + ub + uc}$   
•  $\pi p = \frac{Tu}{u(Th - Tc}) + ub + uc}$   
•  $\pi p = \frac{2uT}{mh(fl+flue-U)} \Rightarrow tric(Uec-U)^{2} + mic(Uec-U)^{2}}$   
•  $\pi p = \frac{2uT}{mh(fl+flue)} + \frac{1}{mic}(ue-U)^{2}}$   
•  $\pi p = \frac{2uT}{mh(fl+flue)} + \frac{1}{mic}(ue-U)^{2}}$   
•  $\pi p = \frac{2uT}{mh(fl+flue)} + \frac{1}{mic}(ue-U)^{2}} \Rightarrow Romjct L Turbayed$   
•  $fleh = Tu + \frac{1}{2mh(1+fl)} \frac{(ue+U)^{2}}{mip qa}} \Rightarrow Turbefon 4 free form
•  $mf(qa)$   
•  $mecholical condition,  $\pi h = \frac{(p+flue-U)^{2}}{mip qa}$   
•  $\pi e^{qa}$   
•  $mcholical condition,  $\pi h = \frac{(p+flue-U)^{2}}{mip qa}$   
•  $\pi e^{qa}$   
•  $mcholical condition,  $\pi h = \frac{(p+flue-U)^{2}}{mip qa}$   
•  $\pi fqa$   
•  $mcholical formult e(Tsp) = Tmax$   
•  $TsFC = mipult/T = \frac{flue}{(Tmin)}$   
•  $fleh = \frac{flue}{\pi (Qa - Cph Tos}}$   
•  $fleh = \frac{flue}{\pi (Qa - Cph Tos}}$   
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